

Introduction to Interferometer and Coronagraph Imaging

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Goals of this talk:

1. Learn to think in terms of wavelets.
2. Learn how to calculate the interference of wavefronts for any optical system.
3. Learn how to separate astrophysical from instrumental effects.
4. Hear about coronagraphs and speckles.

Note: We discuss optical methods ($\lambda < 10 \mu\text{m}$) of wavefront detection here (homodyne detection).

We do not discuss radio methods (heterodyne detection).

Photons and Waves

Basic photon-wave-photon process

We see **individual photons**. Here is the **life history** of each one:

Each photon is emitted by a **single atom** somewhere on the star.

After emission, the photon acts like a **wave**.

This wave expands as a **sphere**, over 4π steradians (Huygens).

A portion of the wavefront enters our telescope **pupil(s)**.

The wave follows **all possible paths** through our telescope

(Huygens again).

Enroute, its **polarization on each path** may be changed.

Enroute, its **amplitude on each path** may be changed,

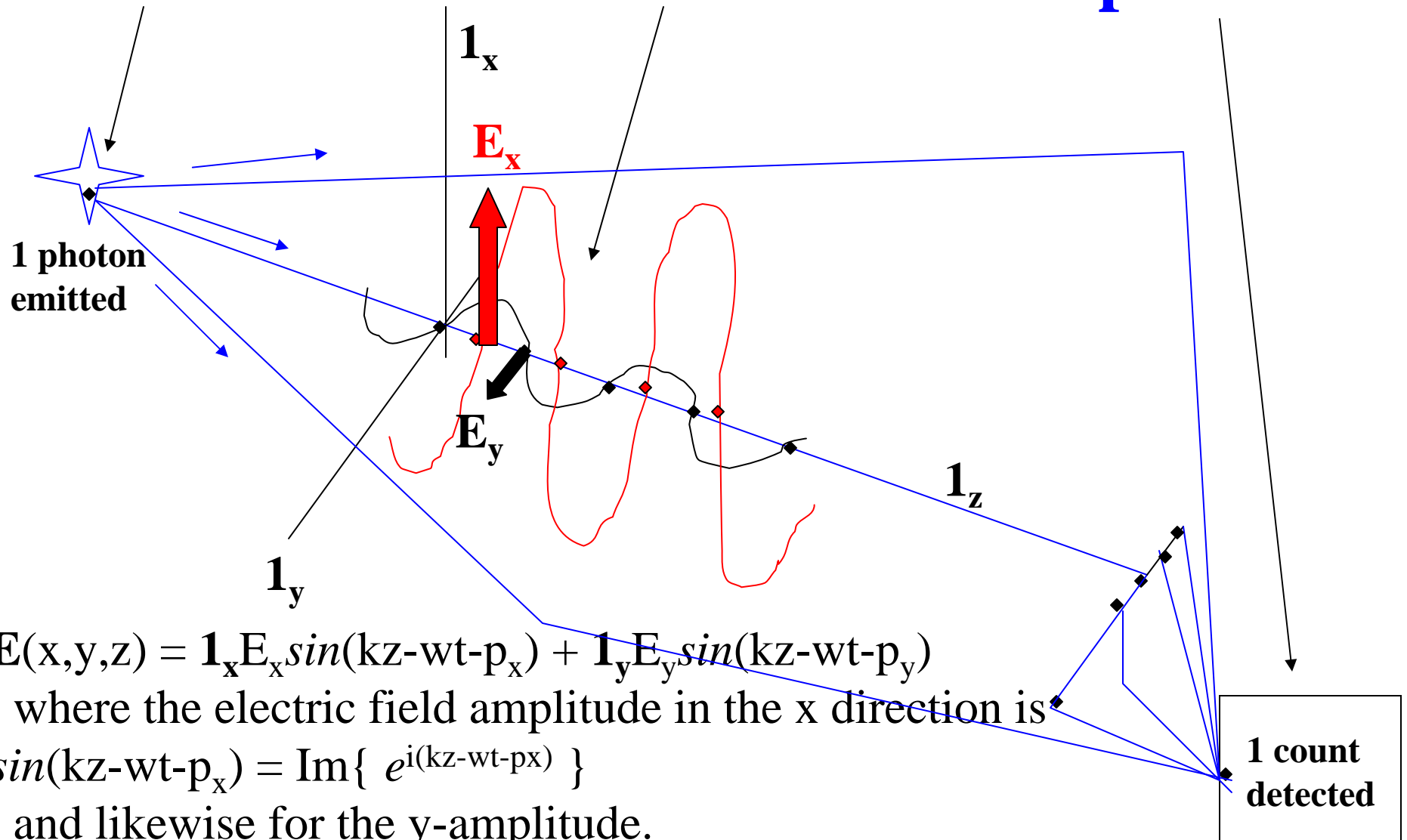
Enroute, its **phase on each path** may be changed.

At each possible detector, the wave “senses” that it has followed these **multiple** paths.

At each detector, the electric fields from all possible paths are **added**, with their polarizations, amplitudes, and phases.

Each detector has **probability** = amplitude² to detect the photon.

Photon.....wave.....photon



$$\mathbf{E}(x,y,z) = \mathbf{1}_x E_x \sin(kz - \omega t - p_x) + \mathbf{1}_y E_y \sin(kz - \omega t - p_y)$$

where the electric field amplitude in the x direction is

$$\sin(kz - \omega t - p_x) = \text{Im} \{ e^{i(kz - \omega t - p_x)} \}$$

and likewise for the y-amplitude.

At detector, *add the waves from all possible paths.*

Fourier optics vs geometric optics

Fourier optics (or physical optics) describes ideal diffraction-limited optical situations (coronagraphs, interferometers, gratings, lenses, prisms, radio telescopes, eyes, etc.):

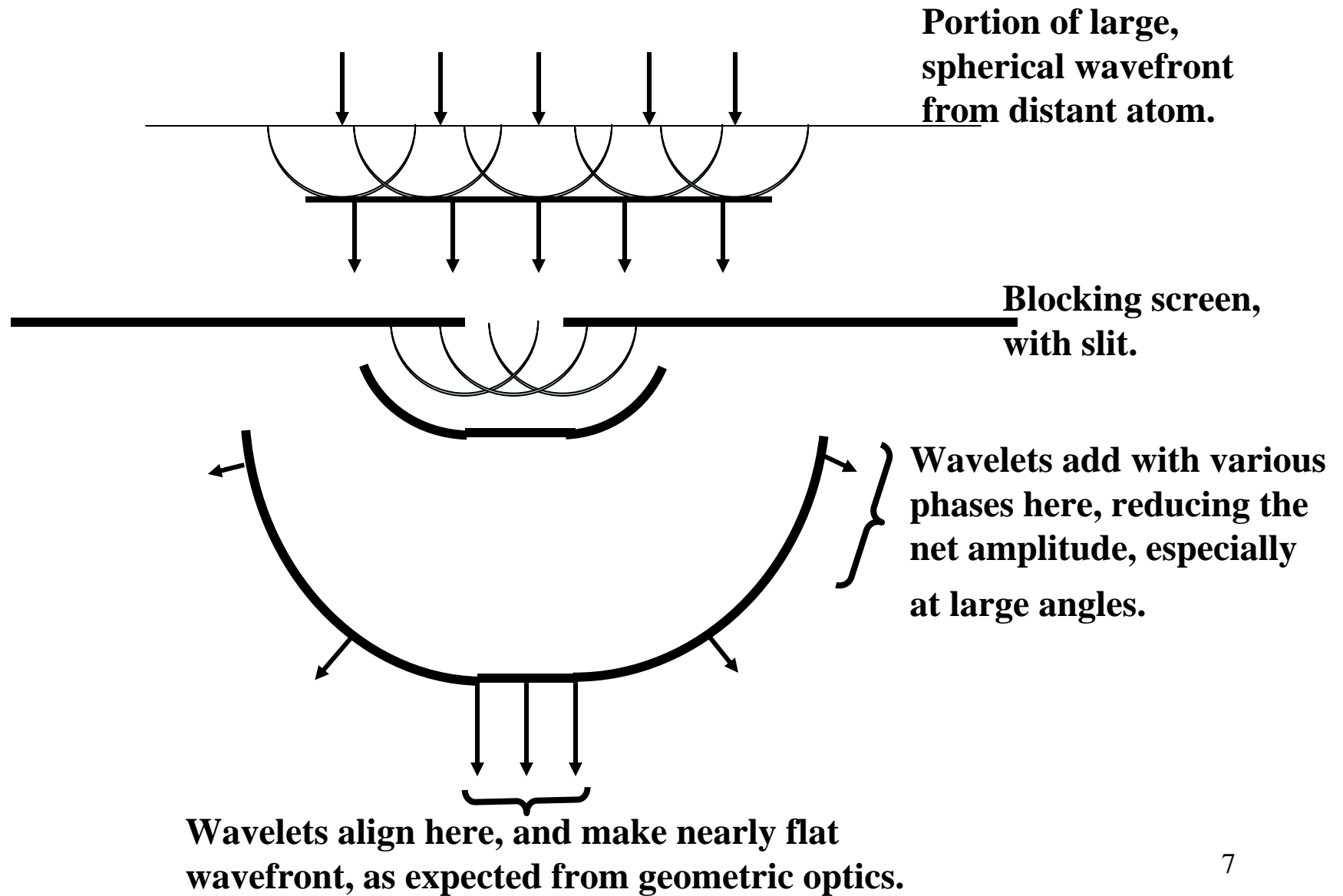
If the all photons start from the same atom, and follow the same many-fold path to the detectors, with the same amplitudes & phase shifts & polarizations, then we will see a diffraction-controlled interference pattern at the detectors.

In other words, **waves** are needed to describe what you see.

Geometric optics describes the same situations but in the limit of zero wavelength, so no diffraction phenomena are seen.

In other words, **rays** are all you need to describe what you see.

Huygens wavelets



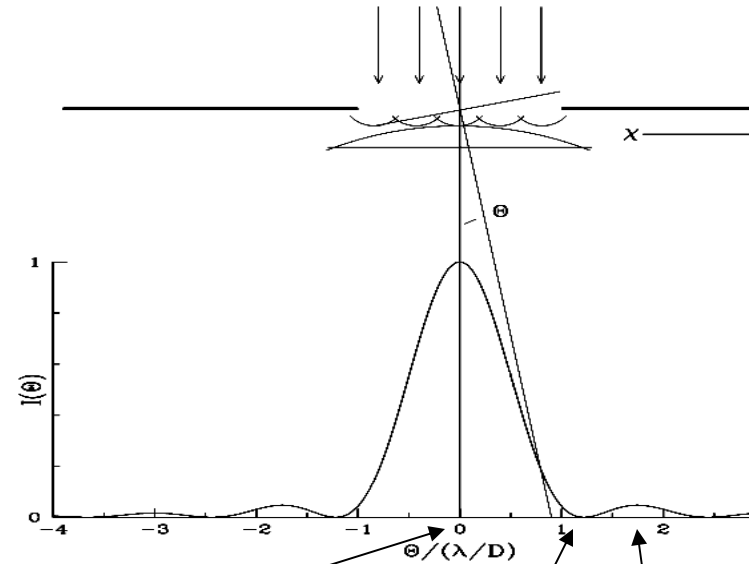
Huygens' wavelets --> Fraunhofer --> Fourier transform

The phase of each wavelet on a surface
Tilted by $\theta = x/f$ and focused by the
Lens at position x in the focal plane is

$$\begin{aligned}\phi(x) &= 2\pi x \sin(\theta) / \lambda \\ &\simeq 2\pi x \theta / \lambda\end{aligned}$$

The sum of the wavelets across the
potential wavefront at angle θ is

$$\begin{aligned}A_{tel}(\theta) &= \sum(\text{wavelets}) \\ &= \int_{pupil} e^{i\phi(x)} dx \\ &= \int_{-D/2}^{+D/2} e^{i(2\pi x \theta / \lambda)} dx \\ &= \frac{\lambda}{2\pi i \theta} \left[e^{+i\pi \theta D / \lambda} - e^{-i\pi \theta D / \lambda} \right] \\ &= \frac{\sin(\pi \theta D / \lambda)}{\pi \theta D / \lambda} D\end{aligned}$$



All waves add in phase here

The net amplitude is zero here

The net amplitude mostly
cancels, but not exactly,
here

Fourier relations: pupil and image

We see that an ideal lens (or focussing mirror) acts on the amplitude in the **pupil plane**, with a **Fourier-transform** operation, to generate the amplitude in the **image plane**.

A second lens, after the image plane, would convert the **image-plane** amplitude, with a second **Fourier-transform**, to the plane where the initial **pupil is re-imaged**.

A third lens after the **re-imaged pupil** would create a **re-imaged image** plane, via a third **FT**.

At each stage we can **modify the amplitude** with masks, stops, polarization shifts, and phase changes. These all go into the **net transmitted** amplitude, before the next FT operation.

Summation of wavelets

Born and Wolf (7th edition, p. 428) define the wavelet summation integral as the Fourier-transform relation between amplitude in the pupil $A_{in}(x,y)$ and amplitude in the focal plane $A_{out}(u,v)$.

Image amplitude = Sum of wavelet amplitudes

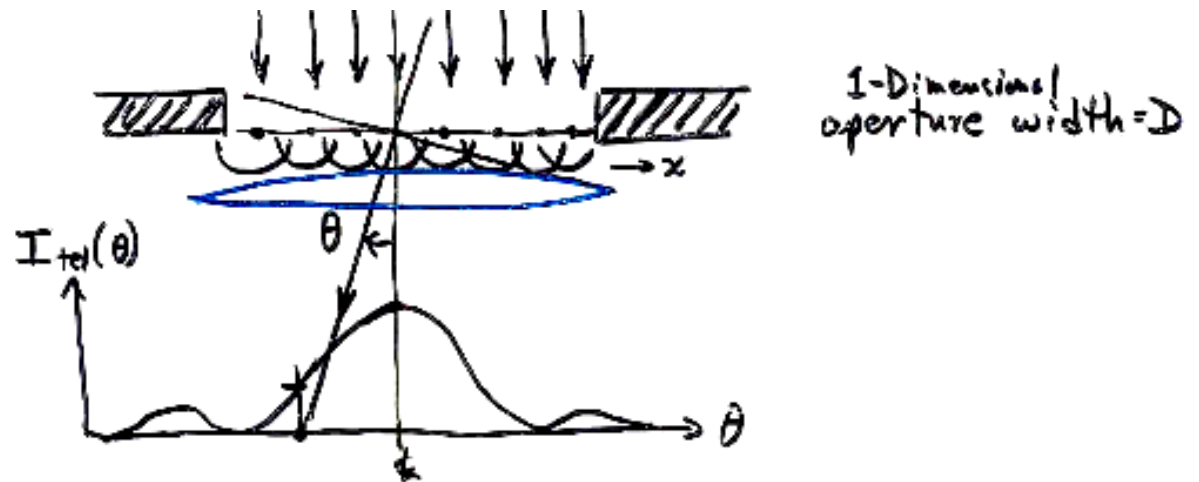
$$A_{out}(u,v) = \frac{1}{\lambda f} \int A_{in}(x,y) e^{-ik(xu+yv)/f} dx dy$$

where

$$|A(x,y)|^2 = \text{energy / area} = \text{Intensity}$$

Simplify: (1) 2D→1D; (2) coef.= 1; (3) $u/f = \theta =$ angle in focal plane.

Derive
single-
telescope
response to
point source



amplitude. $A_{tel}(\theta) = \sum_{\text{wavelets}} = \int_D e^{i(\text{phase at } x)} dx$

$$= \int_{-D/2}^{+D/2} e^{i(2\pi \frac{x\theta}{\lambda})} dx / \int dx$$

$$= \frac{\lambda}{2\pi i \theta} [e^{+i\pi\theta D/\lambda} - e^{-i\pi\theta D/\lambda}] / D$$

$$= \frac{\sin(\pi\theta D/\lambda)}{(\pi\theta D/\lambda)}$$

intensity. $I_{tel}(\theta) = |A_{tel}|^2 = \left[\frac{\sin(\pi\theta D/\lambda)}{\pi\theta D/\lambda} \right]^2$

1st zero. $I_{tel}(\theta_{tel}) = 0$ when $\theta_{tel} = \lambda/D$

circular aperture. $\int_{\text{circle}} \dots \Rightarrow I_{tel}(\theta) = \left[\frac{2J_1(\pi\theta D/\lambda)}{\pi\theta D/\lambda} \right]^2$

$$\theta_{tel} = 1.22 \lambda/D$$

Single telescope again

add constant phase ϕ .

$$A_{tel}(\theta) = \int_{-D/2}^{+D/2} e^{i(2\pi \frac{x\theta}{\lambda} + \phi)} dx \quad / \int dx = \frac{\sin(\pi \theta D/\lambda)}{\pi \theta D/\lambda} \cdot e^{i\phi}$$

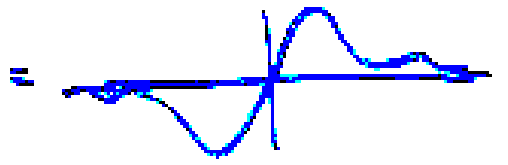
I_{tel} is unchanged.

add off-axis angle θ_0 .

$$A_{tel}(\theta) = \int_{-D/2}^{+D/2} e^{i(2\pi x(\theta + \theta_0)/\lambda)} dx \quad / \int dx = \frac{\sin(\pi(\theta - \theta_0)D/\lambda)}{\pi(\theta - \theta_0)D/\lambda}$$

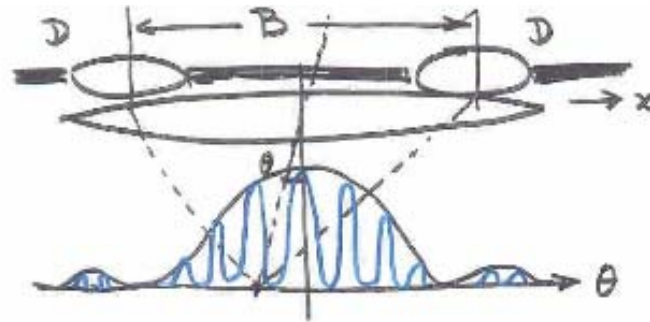
I_{tel} is shifted to center at θ_0 .

add phase step (across $1/2$ aperture) of π .

$$A_{tel}(\theta) = \left[\int_0^{+D/2} e^{i(2\pi x\theta/\lambda)} dx + \int_{-D/2}^0 e^{i(2\pi x\theta/\lambda - \pi/2)} dx \right] / i$$


$$I_{tel}(\theta) = \text{graph of intensity} \quad \text{i.e. 2 speckles.}$$

Derive interferometer (2-tel.) response



amplitude. $A_{\text{int}}(\theta) = \sum_{\text{wavelets}} = \int e^{i(\text{phase at } x)} dx$

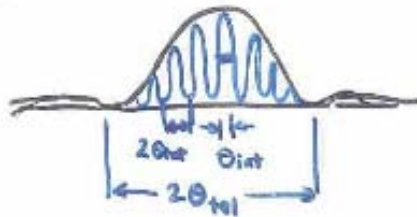
$$= \left[\int_{+\frac{1}{2}B - \frac{1}{2}D}^{+\frac{1}{2}B + \frac{1}{2}D} + \int_{-\frac{1}{2}B - \frac{1}{2}D}^{-\frac{1}{2}B + \frac{1}{2}D} \right] / 2D$$

$$= \frac{\sin(\pi\theta D/\lambda)}{\pi\theta D/\lambda} \cdot \cos(\pi\theta B/\lambda)$$

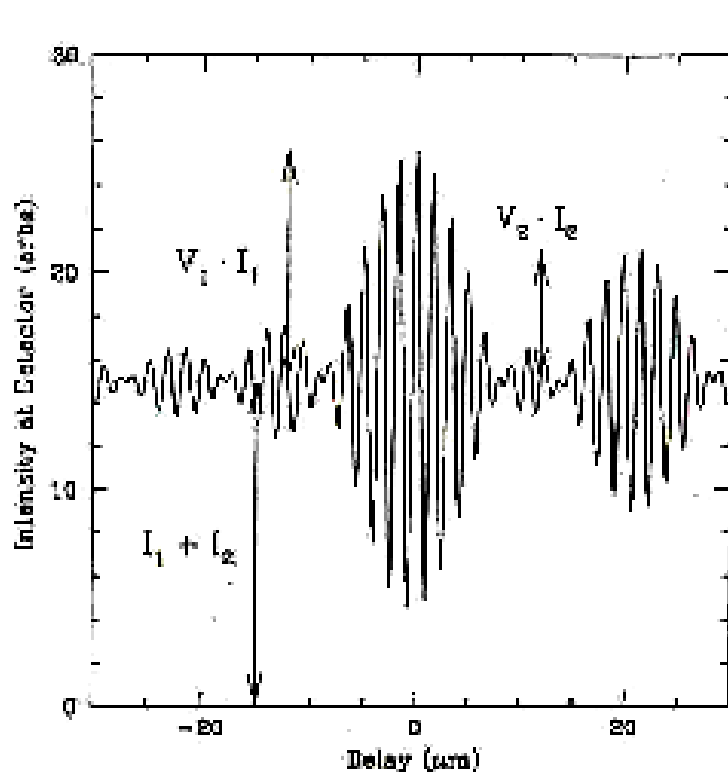
intensity. $I_{\text{int}}(\theta) = I_{\text{tel}}(\theta) \cdot \frac{1}{2} [1 + \cos(2\pi\theta B/\lambda)]$

1st zero. $I_{\text{int}}(\theta_{\text{int}}) = 0$ when $\theta_{\text{int}} = \frac{\lambda}{2B}$ = width of fringe.

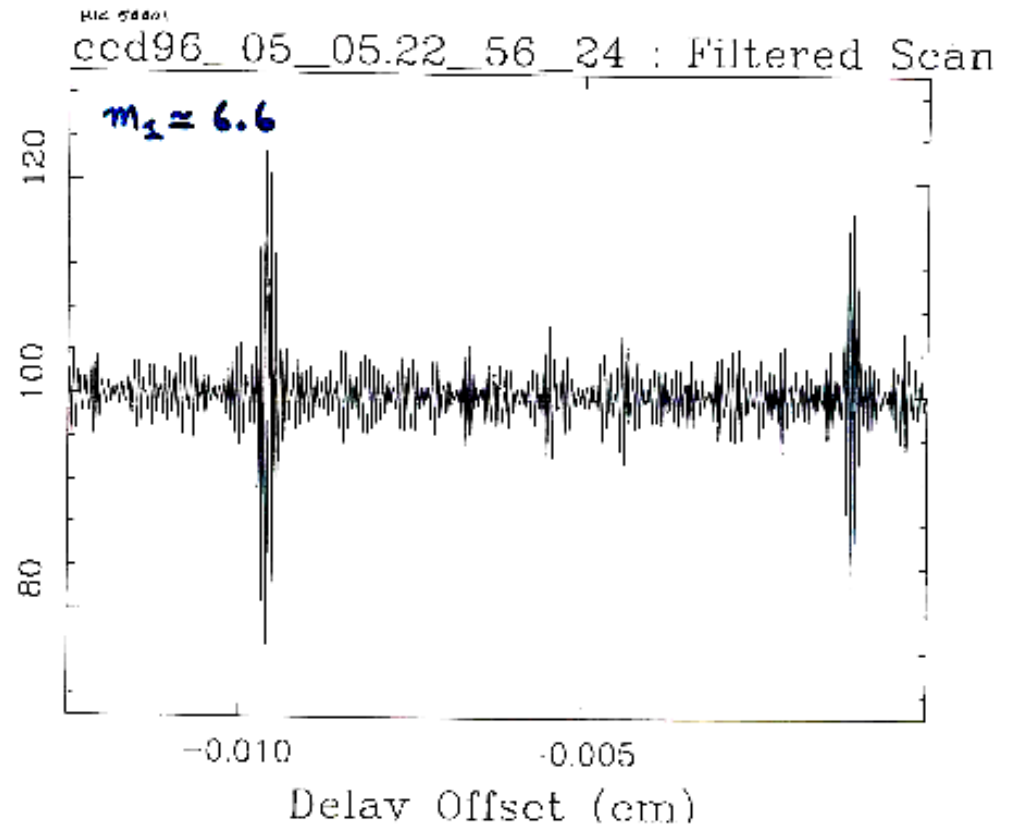
number of fringes in packet. $(\text{no. fringes}) = \frac{2\theta_{\text{tel}}}{2\theta_{\text{int}}} = \frac{1.22\lambda/D}{0.50\lambda/B} = 2.44 \frac{B}{D}$



Binary star interferograms



Model interferogram for a binary star, with well-separated fringe packets.



Observed interferogram of a very wide-spaced binary. CCD detector, no filter, IOTA interferometer, 1996 data.

Derive uniform disk response

Add up (incoherent) fringe patterns from ^{square} disk =

intensity.
$$I_{USD}(\theta) = \sum_{\text{sq. disk}} (\text{intensities}) = \int_{\text{sq. disk}} I_{\text{int}}(\theta - \theta_x) \cdot d\theta_x d\theta_y / \int d\ell$$

$$= \int_{-\theta_{\text{disk}}/2}^{+\theta_{\text{disk}}/2} I_{\text{tel}}(\theta) \cdot \frac{1}{2} [1 + \cos 2\pi(\theta - \theta_x) B/\lambda] \cdot \theta_{\text{disk}} \cdot d\theta_x / \theta_{\text{disk}}^2$$

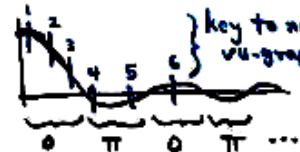
$$\approx I_{\text{tel}}(\theta) \cdot \frac{1}{2} \left[1 + \underbrace{\left(\frac{\sin \pi B \theta_{\text{disk}} / \lambda}{\pi B \theta_{\text{disk}} / \lambda} \right)}_{V_{USD}} \cdot \cos \frac{2\pi \theta B}{\lambda} \right]$$

visibility.
$$V_{USD} = \frac{\sin(\pi B \theta_{\text{disk}} / \lambda)}{\pi B \theta_{\text{disk}} / \lambda}, \text{ square disk.}$$

$$V_{UD} = \frac{2 J_1(\pi B \theta_{\text{disk}} / \lambda)}{\pi B \theta_{\text{disk}} / \lambda}, \text{ round disk.}$$

1st zero. $V_{UD} = 0$ when $\theta_{\text{disk}} = 1.22 \lambda / B$, $B = 1.22 \lambda / \theta_{\text{disk}}$

phase. phase = $\begin{cases} 0 & \text{inside odd lobes} \\ \pi & \text{inside even lobes} \end{cases}$



example 1. see next vu-graph from Born & Wolf.

example 2. SIM pocket demonstration card.



$$D \approx 0.07 \text{ mm} \quad \text{so} \quad \theta_{\text{tel}} = 1.22 \lambda / D \approx 2000. \mu \text{rad} \approx \text{sun, moon.}$$

$$B \approx 0.25 \text{ mm} \quad \text{so} \quad \theta_{\text{int}} = \frac{\lambda}{2B} \approx 200. \mu \text{rad} \approx \text{Mag-light at } \frac{1}{6} \text{ inches.}$$

$$(\# \text{ fringes in packet}) = 2.44 B/D \approx 8.$$

Uniform disk: interferograms

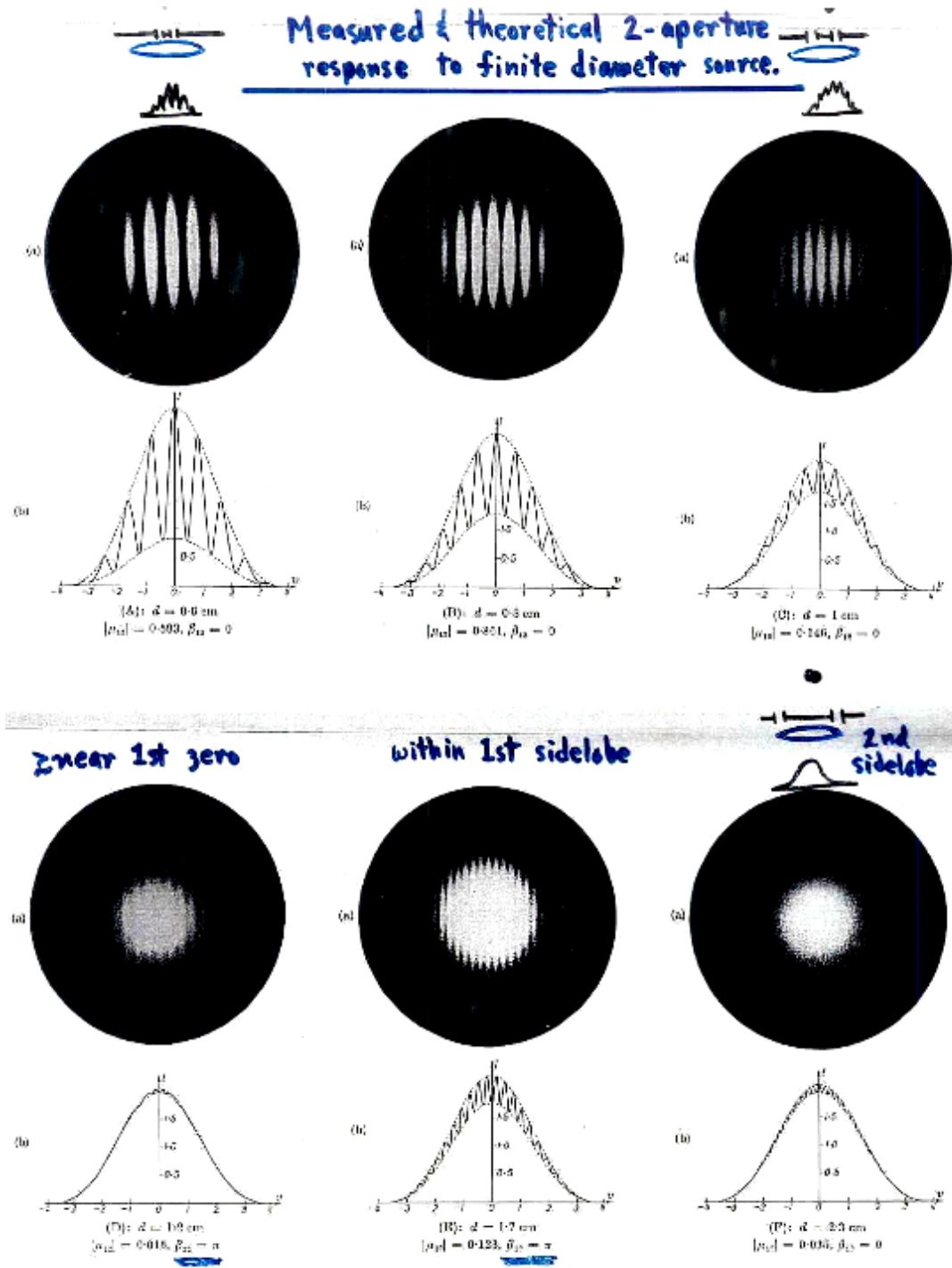


Fig. 10.6. Two-beam interferes with partially coherent light.

Van Cittert-Zernike theorem

Beam pattern on sky.

Think like a radio astronomer.

The antenna pattern is considered to be projected out from the receiver horn & antenna & array onto the sky. As you move the antenna, or change the phase at an array element, the pattern sweeps across the sky. The received signal is the convolution of the moving pattern and the sources in the sky.

A sinusoidal pattern picks out the Fourier component at that spacing of fringes.

van Cittert - Zernike theorem (1934, 1938).



Complex degree of coherence.

$$\mu_{12}(\vec{B}) = \frac{\int_{\text{FOV}} I(\vec{\alpha}) \cdot e^{-ik\vec{B}\cdot\vec{\alpha}} \cdot d\vec{\alpha}}{\int_{\text{FOV}} I(\vec{\alpha}) \cdot d\vec{\alpha}}$$

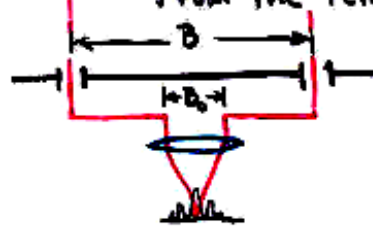
degree of coherence. $|\mu| \equiv V = \text{visibility}$; phase = $\arg(\mu)$.

inverse relation.

$$I(\vec{\alpha}) / \int_{\text{FOV}} I(\vec{\alpha}) d\vec{\alpha} = \int_{\text{all } \vec{B}} \mu(\vec{B}) \cdot e^{+ik\vec{B}\cdot\vec{\alpha}} \cdot d\vec{B}$$

Michelson's stellar interferometer

Suppose we decouple the collecting apertures at B from the telescope feed apertures at B_0 .



The coherence is measured by B.
The display pattern is set by B_0 .

$$I_{int}(\theta) = \underbrace{I_{tel}(\theta)}_{\text{envelope vs } \theta} \cdot \frac{1}{2} \left[\underbrace{1 + \left(\frac{\sin \pi B \theta_{disk} / \lambda}{\pi B \theta_{disk} / \lambda} \right)}_{\text{degree of modulation indep. of } \theta} \cos \left(\underbrace{2\pi \theta B_{tel} / \lambda}_{\text{modulation vs } \theta \text{ with period indep. of } B \text{ and } \theta_{disk}} \right) \right]$$

magnification. So can make B_0 any convenient value. Michelson used $B_0 = 1.14$

so the fringe width is $\theta_{int} = \frac{\lambda}{2B_0} = 0.045$ arcsec.

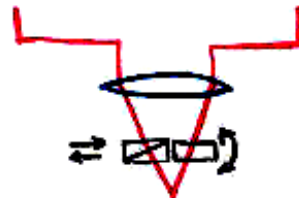
Assume his eye had $\theta_{eye} \approx 1.22 \frac{\lambda}{5 \text{ mm}} = 25$ arcsec.

Magnify θ_{int} to match θ_{eye} with eyepiece M,

$$M = \theta_{eye} / \theta_{int} \approx \frac{25}{.045} \approx 600.$$



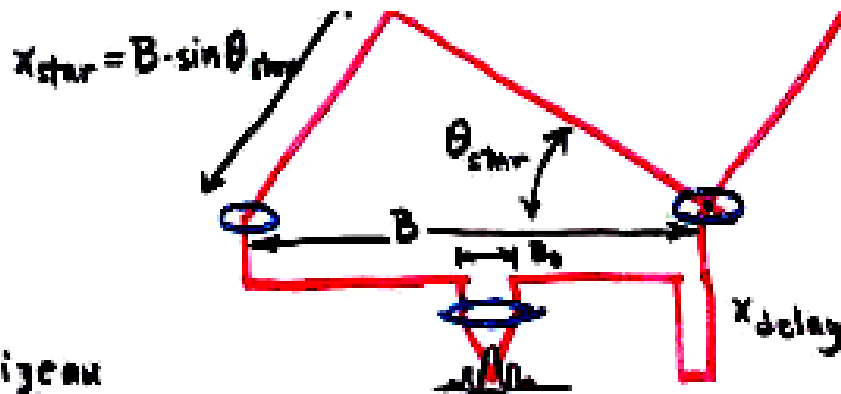
details.



Tilt plate gives angle motion,
& superposes images,
ie., makes wavefronts parallel at entrance pupil.

Wedge plates give variable thickness,
to compensate for tilt plate's thickness,
ie., makes all color wavefronts arrive at same time
as in other beam.

Image-plane interferometer



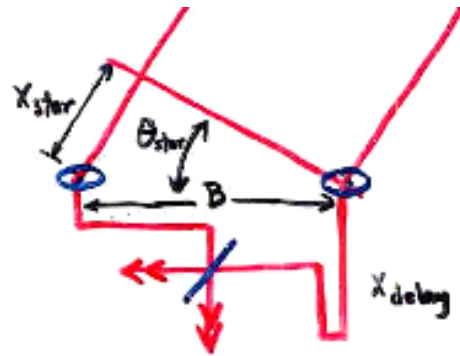
Phase difference between beams

$$\phi = \frac{2\pi}{\lambda} (x_{\text{delay}} - x_{\text{star}})$$

Fizeau
type.

$$I_{\text{int}}(\theta) = \underbrace{I_{\text{tot}}(\theta)}_{\text{envelope vs } \theta} \cdot \frac{1}{2} \left[\underbrace{1 + V}_{\text{visib. of star}} \cdot \cos \frac{2\pi}{\lambda} \left(\underbrace{\theta B_0}_{\text{fringe modulation}} + \underbrace{x_{\text{delay}} - x_{\text{star}}}_{\text{fringe phase or position.}} \right) \right]$$

Pupil-plane interferometer



Phase difference between beams

$$\phi = \frac{2\pi}{\lambda} (X_{\text{delay}} - X_{\text{star}}) + \frac{\pi}{2}$$

conservation of energy
at lossless beamsplitter

Michelson
type.

$$I_{\text{int}}(t) = I_{\text{tel}}(\theta) \cdot \frac{1}{2} \left[1 \pm V \cdot \sin \frac{2\pi}{\lambda} (X_{\text{delay}} - X_{\text{star}}) \right]$$

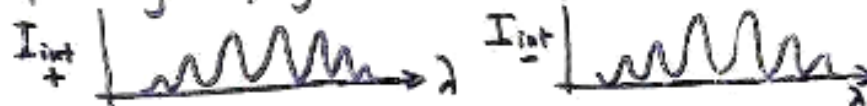
Note: B_0 here is zero; use time modulation $X_{\text{delay}}(t) - X_{\text{star}}(t) = v \cdot t$

and 1 pixel each for I_{\pm} .

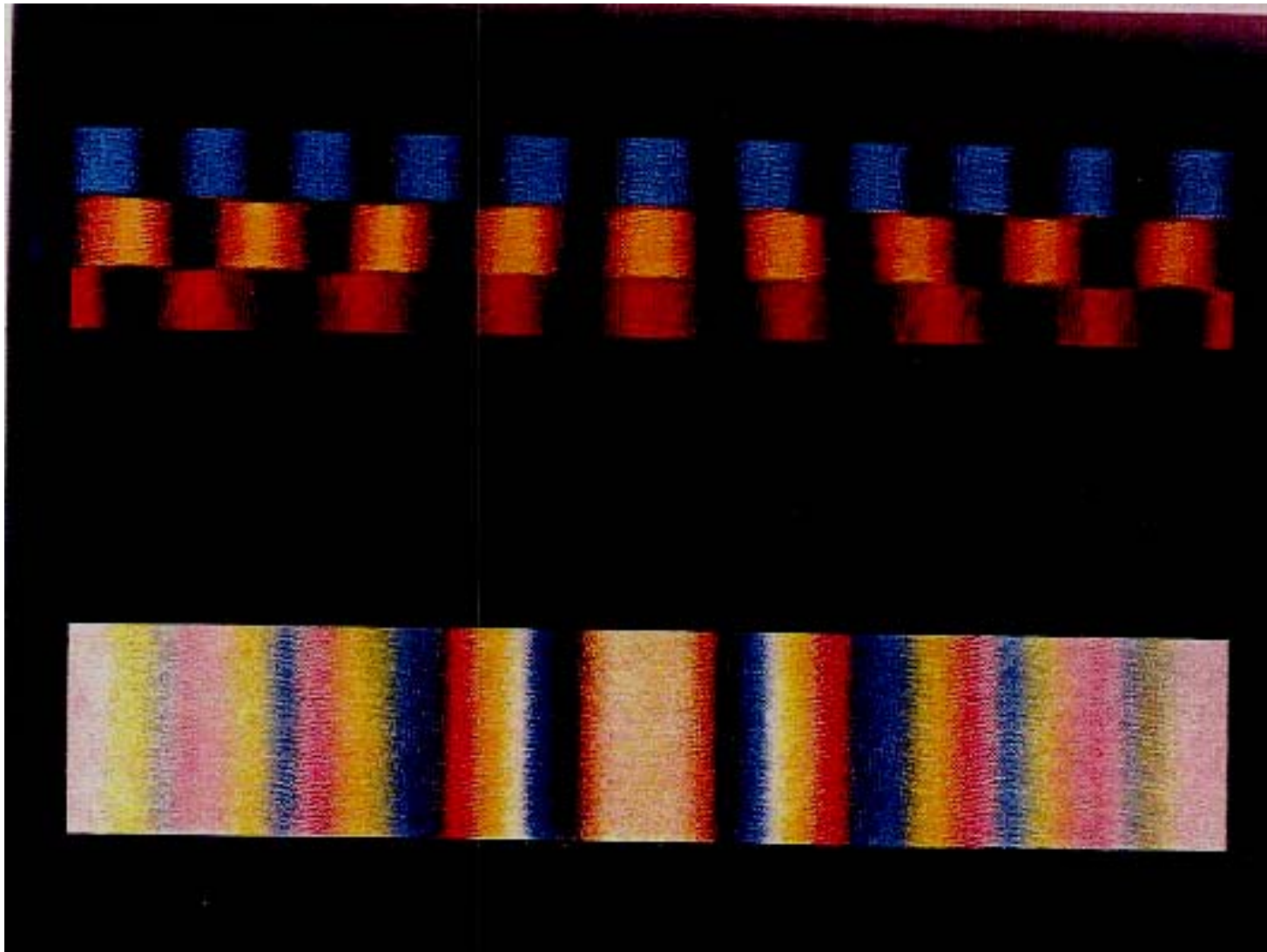


Channel
spectrum.

Spatially display each wavelength segment of I_{int} , with delay \approx few λ .



Colors in interferogram

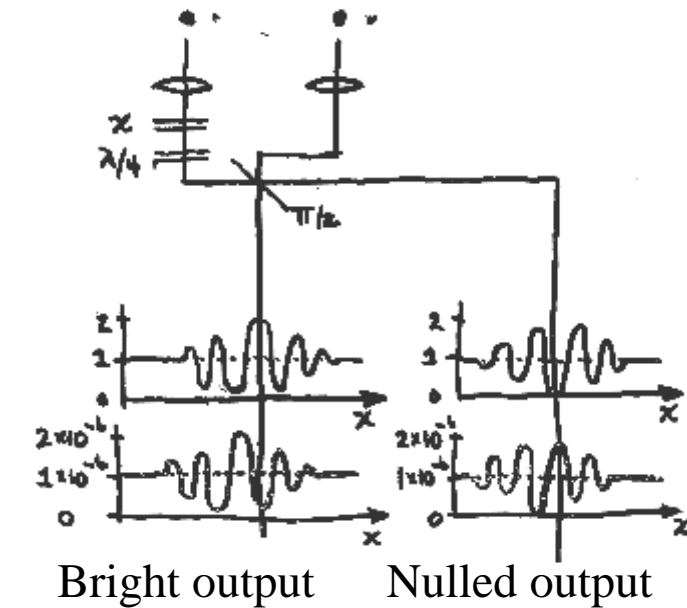


Nulling

Nulling interferometer (Bracewell)

Star:

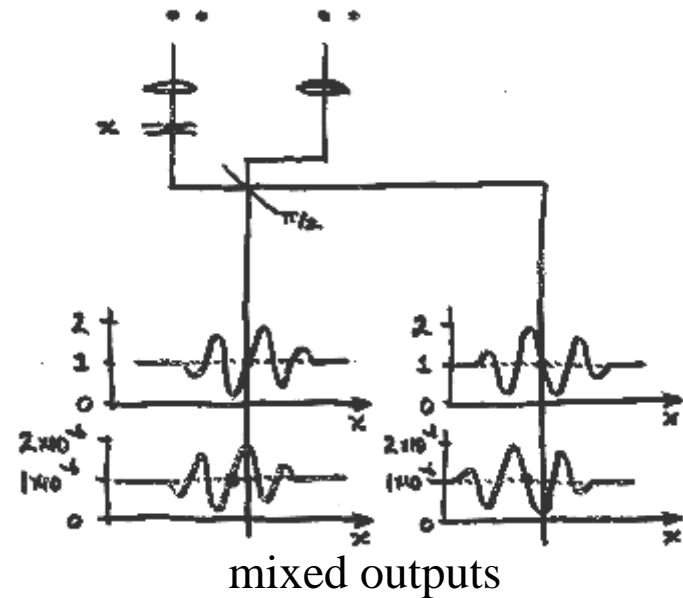
Planet:



Stellar interferometer (Michelson)

Star:

Planet:



Standard Nulling

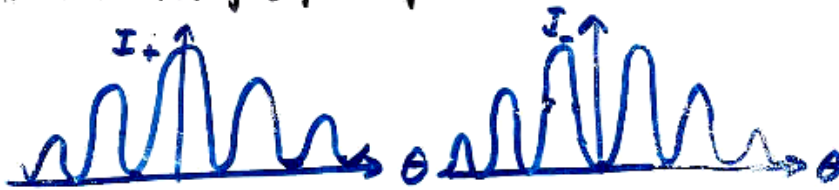


Assume that an ideal achromatic null can be arranged. Then the intensity is

$$I_{\pm} = |e^{ik\theta r} \pm e^{-ik\theta r}|^2$$

$$= 2 \cdot [1 \pm \cos 2k\theta r]$$

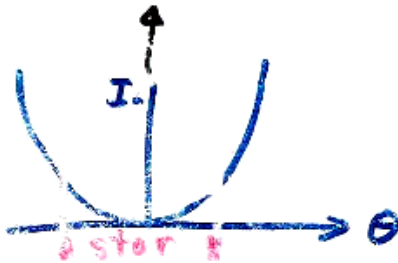
The complementary outputs are the bright & null fringes, resp.



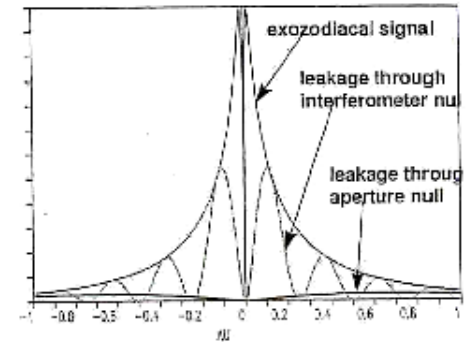
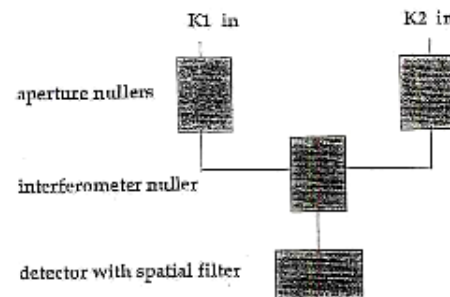
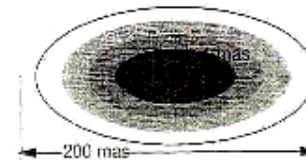
Near the null, the intensity is quadratic

$$I_-(\theta) \approx 2 \cdot \left[1 - \left(1 - \frac{(2k\theta r)^2}{2!} + \dots \right) \right]$$

$$\approx (2k\theta r)^2 - \dots$$



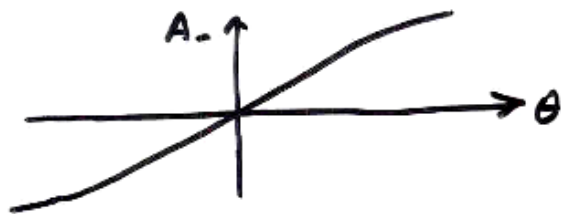
Theta² nulling



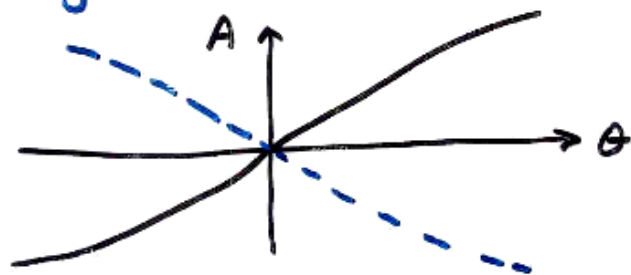
Theta⁴ nulling

The amplitude (electric vector) in a standard null is

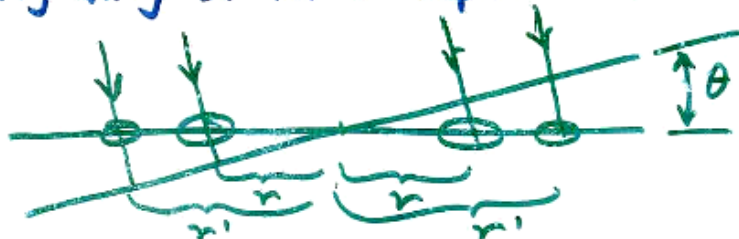
$$A_- = e^{+ik\theta r} - e^{-ik\theta r} = 2i \cdot \sin(k\theta r)$$



If we could cancel this amplitude with one of opposite sign, we could make a very wide null.



Try using 2 more apertures:



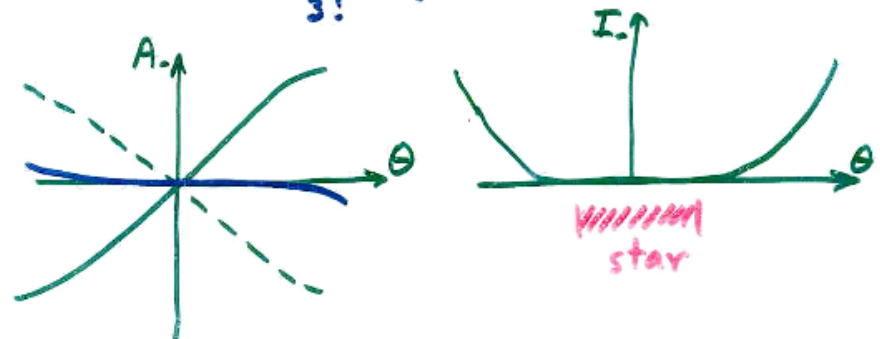
The amplitude from all 4 apertures is, assuming the outer ones have relative weight ϵ :

$$A_- = \epsilon e^{+ik\theta r'} + e^{+ik\theta r} - e^{-ik\theta r} - (\epsilon e^{-ik\theta r'}) = 2i \cdot \{ \sin(k\theta r) - \epsilon \sin(k\theta r') \}$$

where we have added exactly π retardation to flip the sign.

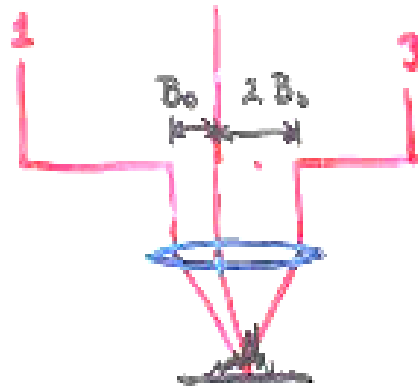
$$A_- \approx \underbrace{k\theta(r - \epsilon r')} - \frac{(k\theta)^3}{3!} (r^3 - \epsilon r'^3) + \dots = 0 \text{ if } \epsilon = r/r'$$

$$\text{Then } A_- \approx -\frac{(k\theta r)^3}{3!} (1 - 1/\epsilon^2) + \dots$$



So 2 extra mirrors, or petals, will work, provided that phase control exists.

Multiplexing in the image plane

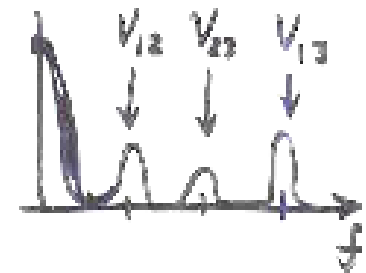


Use minimum redundancy array at combiner lens.

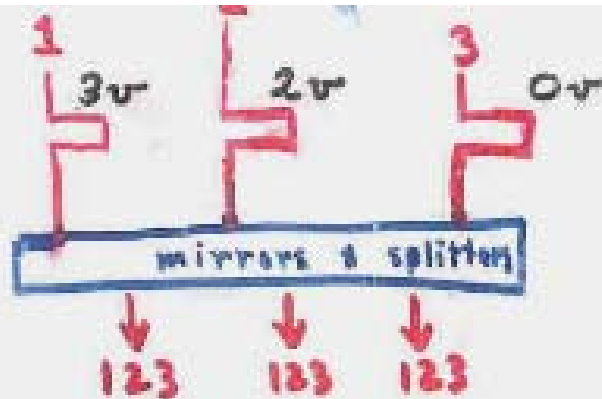
Get different spatial frequency for each baseline.

Figure type.

$$|\text{FFT}(\text{fringe pattern})|^2 = \text{power spectral density}$$



Multiplexing in the pupil plane

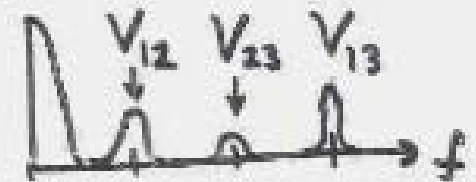


Use different delay-line speeds.

Mix beams & get different time frequencies in each.

Michelson
type.

$$|\text{FFT (each time sequence)}|^2 = \text{power}$$



FOV.

The schemas above have a $\text{FOV} < \Theta_{\text{tel}}$, i.e. small, because output pupils \neq scaled input pupils.

Golden rule

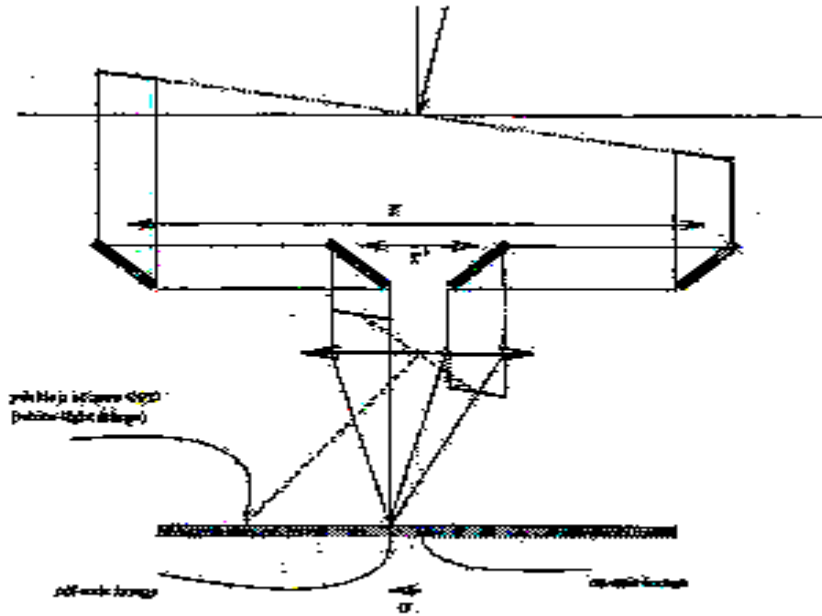
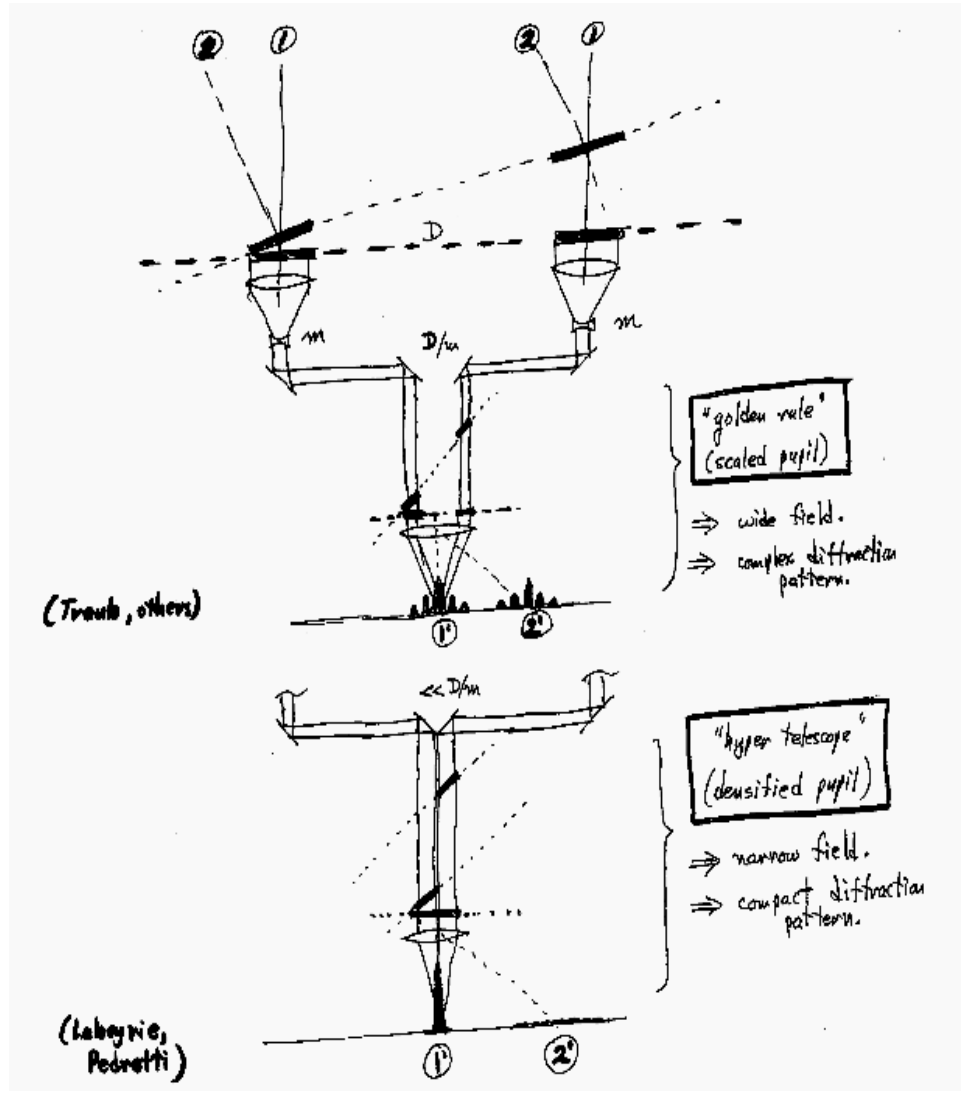


Figure 4.9: Geometry for 2 element Michelson interferometer.

Output pupil must be a scaled version of input pupil in order to obtain a wide field of view.



Pupil densification

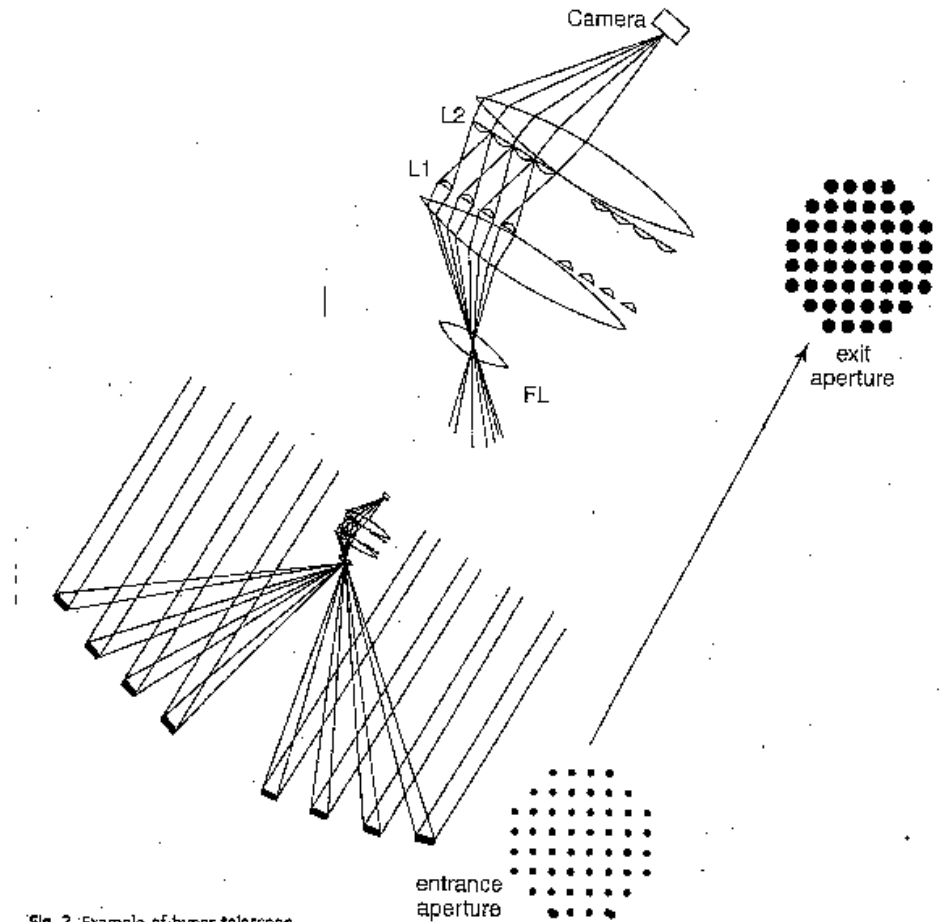


Fig. 2. Example of hyper-telescope optics. Multiple mirrors form a sparse paraboloidal giant mirror, and a lens (FL) in the focal plane forms a pupil image on a pair of lens arrays L1 and L2, having short and long focal lengths, respectively. This setup enlarges the subpupils in the exit aperture compared to those in the entrance aperture, producing a usable image on the camera.

Instrumental effects: 1

Bandpass. If rectangular bandpass of width $\Delta\sigma$ (where $\sigma = \frac{1}{\lambda}$),
then $V_{\text{bandpass}} = \frac{\sin \pi \cdot \alpha \cdot \Delta\sigma}{\pi \cdot \alpha \cdot \Delta\sigma}$ where $\alpha \equiv X_{\text{delay}} - X_{\text{star}}$.

Wavefront tilt. If wavefronts are tilted by angle α , then
 $V_{\text{tilt}} = \frac{\sin \pi \cdot D \cdot \alpha / \lambda}{\pi \cdot D \cdot \alpha / \lambda}$ or $\frac{2 J_1(\pi D \alpha / \lambda)}{\pi D \alpha / \lambda}$
square circular

For $V_{\text{tilt}} > 0.90$ need $\alpha < 0.3 \lambda / D$.

Relative intensity. If the relay optics and/or beam combiner have intensity ratio ρ , then
 $V_{\text{rel-int.}} = \frac{2}{\rho^{1/2} + \rho^{-1/2}}$.

Instrumental effects: 2

Non-flatness
of surfaces.

If the wavefronts have rms perturbations δ , then

$$V_{\text{surfaces}} \approx e^{-(2\pi\delta/\lambda)^2}.$$

If there are N surfaces of δ_0 each, then

$$\delta \approx N^{1/2} \cdot \delta_0.$$

If $\delta = \lambda/20$ is rms of each beam, then

$$V(\lambda/20) \approx e^{-(\pi/10)^2} \approx 0.90.$$

Shear.

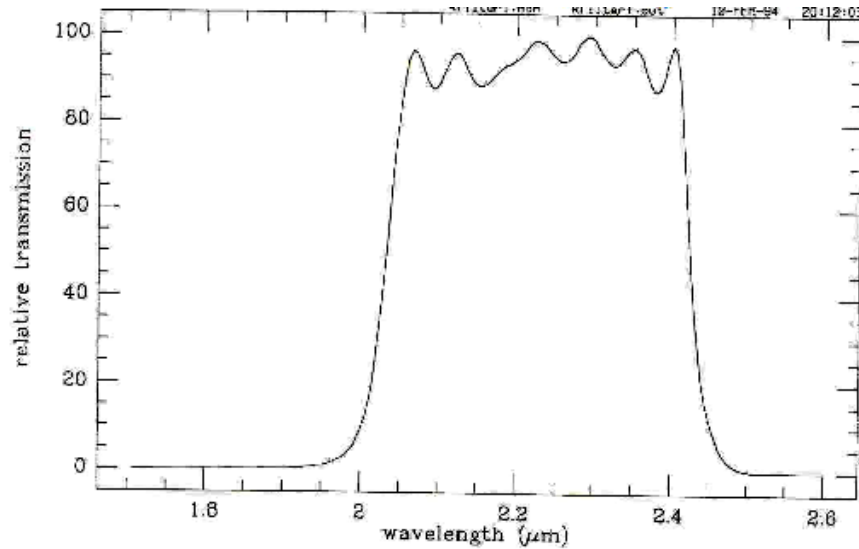
No effect, unless beams no longer overlap.

Different
telescope
diameters.

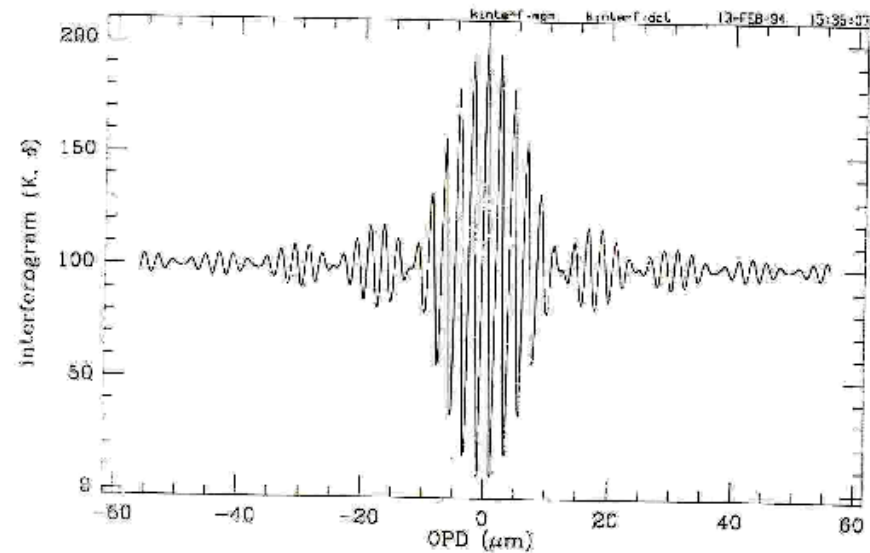
See rel. int. calc.

Filter and interferogram shapes

K-band filter
transmission



K-band
interferogram



Measuring visibility

$\lambda/4$ steps. Change x by $(\lambda/4) \times (0, 1, 2, 3)$, measure $I(x)$,
calculate $V \sim \frac{0-2 + 1-3}{0+1 + 2+3} \frac{\text{wave}}{0+1+2+3}$.

many λ sweep. Change $x = vt$ and repeat in triangle wave.
- fit theoretical wave packet to time data;
- calculate $|FFT|^2$ & ratio high freq. to low;
- wavelet analysis.

dispersed
(channel)
spectrum. Allow atmosphere to give few λ path variation of x
calculate peak-to-valley variations at each λ .

Strehl: 1

Strehl ratio is approximately

$$S = e^{-\phi^2} = \exp(-\phi^2)$$

where ϕ is the rms phase error across a wavefront.

Observed visibility is the product of 3 terms:

$$V_{\text{observed}} = S_{\text{atmos}} S_{\text{instrum}} V_{\text{object}}$$

Instrumental Strehl ratio is the product of many terms:

$$S_{\text{instrum}} = S_{\text{servo}} S_{\text{flat}} S_{\text{align}} S_{\text{diffraction}} S_{\text{flux}} S_{\text{overlap}} S_{\text{vibration}} S_{\text{window}} S_{\text{polarization}}$$

Strehl: 2

Atmospheric variance, with tip-tilt removed by a servo system with bandwidth $\nu/\pi D$, is

$$\varphi^2 = (0.134 + 0.096)(D/r_0)^{5/3}(\lambda_0/\lambda)^2$$

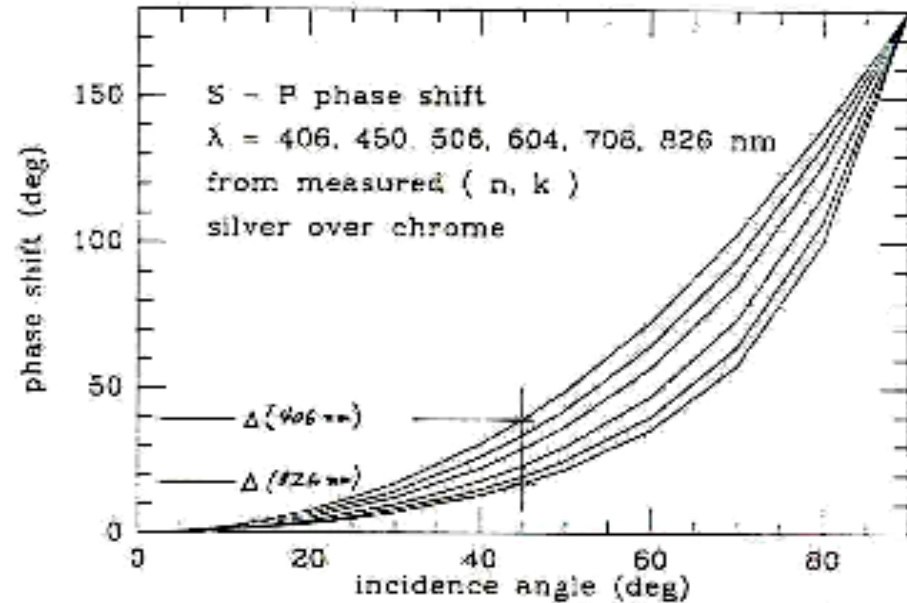
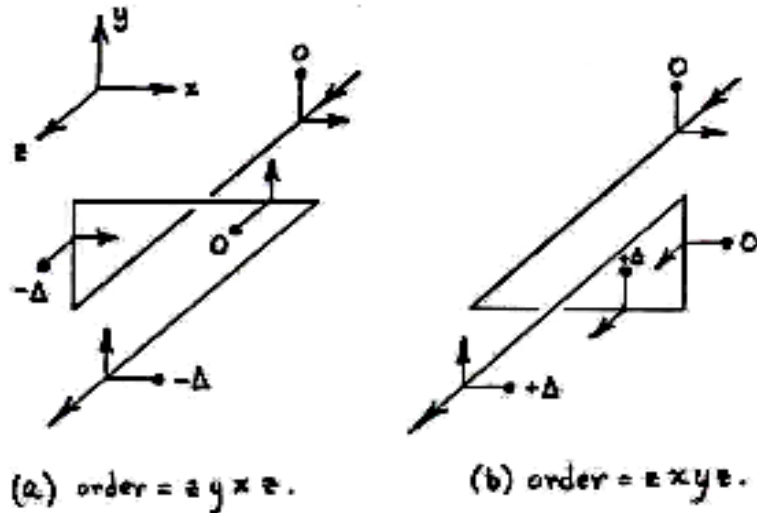
Wavefront flatness variance from mirror surfaces is

$$\varphi^2 = \varphi_1^2 + \dots + \varphi_n^2$$

Mirrors are often specified in terms of surface peak-to-valley where an empirical relation is

$$PV = 5.5 \text{ RMS}$$

Polarization and visibility



S and P refer to the electric vector components perpendicular and parallel to the plane of incidence. For a curved mirror, these axes vary from point to point.

Visibility reduction factor

$$\text{Beam 1: } \vec{A}_1 = (A_x, A_y)_1 = a_1 e^{ik_1 z} (1, e^{i\phi_1})$$

$$\text{Beam 2: } \vec{A}_2 = (A_x, A_y)_2 = a_2 e^{ik_2(z+l)} (1, e^{i\phi_2})$$

$$\text{Combined: } I = |\vec{A}_1 + \vec{A}_2|^2$$

$$I = \bar{I} \cdot \left[1 + \underbrace{\left(\frac{2a_1 a_2}{a_1^2 + a_2^2} \right)}_{\text{visibility term}} \cdot \underbrace{\cos(kl + \frac{\phi}{2})}_{\text{modulation term}} \cdot \underbrace{|\cos \frac{\phi}{2}|}_{\substack{\text{polarization} \\ \text{term} \\ \equiv \text{constant}}} \right]$$

where $\phi \equiv \phi_2 - \phi_1$ = relative phase shift between 2 beams.

- In unpolarized light, the measured visibility can be permanently degraded by purely instrumental polarization effects, in the amount

$$|\cos \frac{\phi}{2}|$$

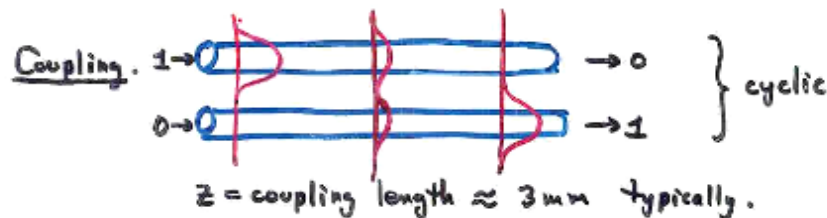
which is a function of wavelength only.

Single-mode fiber optics

Core. $\left\{ \begin{array}{l} \text{Core index } n_1, \text{ radius } a \text{ } (n_1 \sim 1.48, a \sim 2 \mu\text{m}). \\ \text{Cladding index } n_2, \text{ radius } b \text{ } (n_2 \sim 1.46, b \sim 60 \mu\text{m}). \\ \text{Incident/exit cone } \sin i = (n_1^2 - n_2^2)^{1/2} \equiv NA \text{ } (i \sim 14^\circ \\ \text{ } f/2.0) \end{array} \right.$

Dispersion. $\left. \begin{array}{l} - \text{intermodal} = 0 \text{ for SM fiber.} \\ - \text{material} \\ - \text{waveguide} \end{array} \right\} \text{balance these to get zero.}$

Waveguide parameter. $V = \frac{2\pi}{\lambda_0} a (n_1^2 - n_2^2)^{1/2} > 10 \Rightarrow \text{geometric optics}$
 $< 10 \Rightarrow \text{wave optics.}$



Mfg. couplings. $\left. \begin{array}{l} - \text{twist \& melt (fused)} \\ - \text{polish \& mate (polished)}. \end{array} \right.$

Cutoff λ_c . For $\lambda > \lambda_c$ the fiber is single-mode.
 $\lambda_c = \frac{2\pi a}{2.4048} (n_1^2 - n_2^2)^{1/2}. \text{ If } NA \sim .24, \lambda_c \sim 0.6 a.$

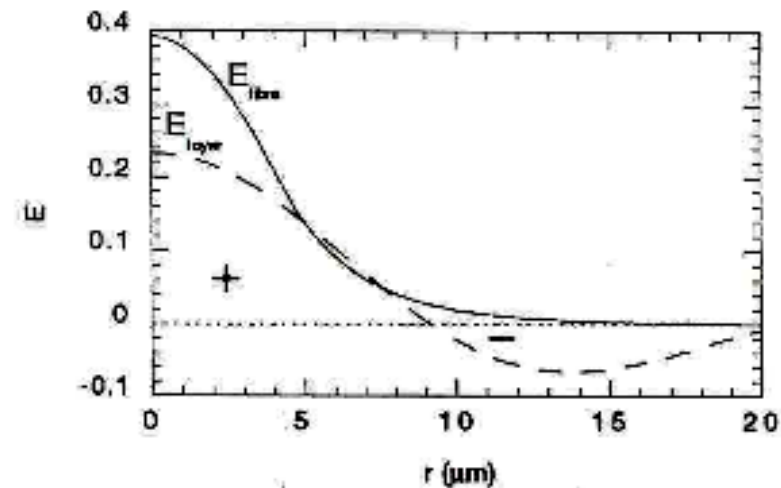
Etendue. $A\Omega = \pi a^2 \pi i^2 = \pi a^2 \pi (NA)^2 \approx (1.202 \lambda_c)^2 \approx \lambda^2.$

Transmission. loss $< 1 \text{ dB/km}$ for silica & fluoride.

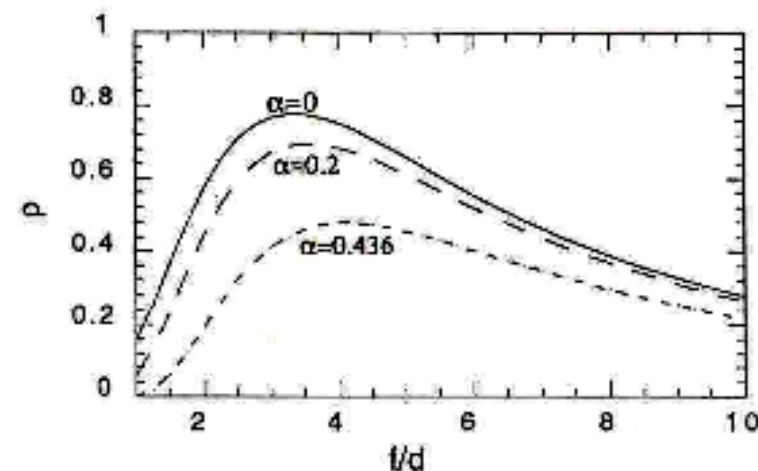
Integrated optics. Fibers on a chip.

Injecting starlight into a fiber

- Efficiency set by the overlap integral:
in the focal plane: $\rho = \left| \iint E_{tel} E_{fibre}^* \right|^2$
=> the field *amplitudes* must match



- The optimal f/d is the one that maximizes the overlap integral
- Maximum possible efficiency: $\rho_{\max} = 78\%$
(but less if the pupil has a central obstruction α)



Integrated optics: 1

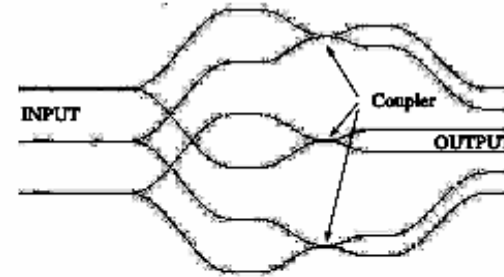
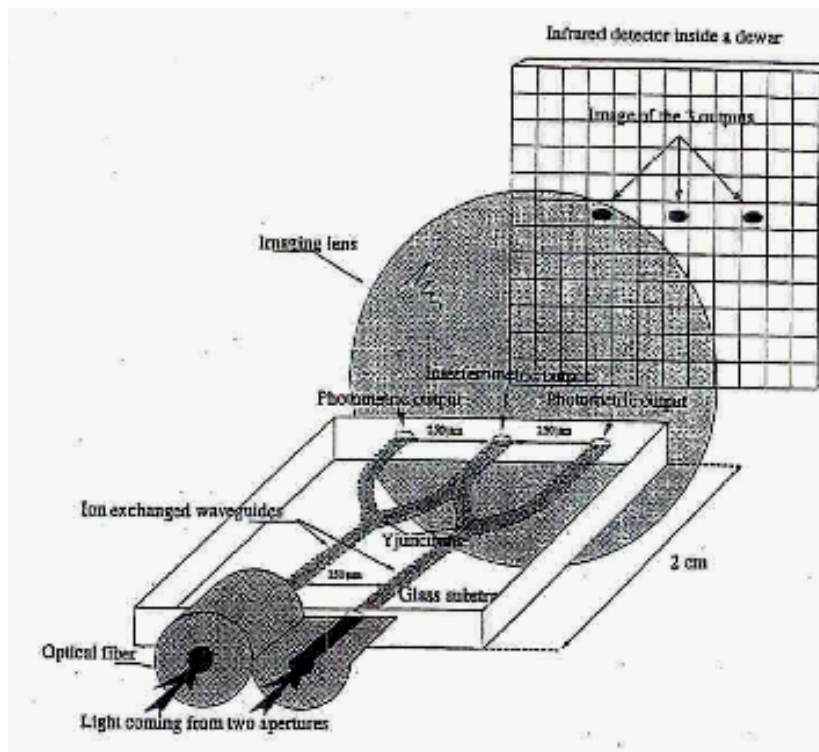


Figure 1. Description of the IONIC-LORA three-way beam combiner. Three inputs are split (ed with Glass "Y" junctions) to provide a pairwise beam combination with another set of three couplers.

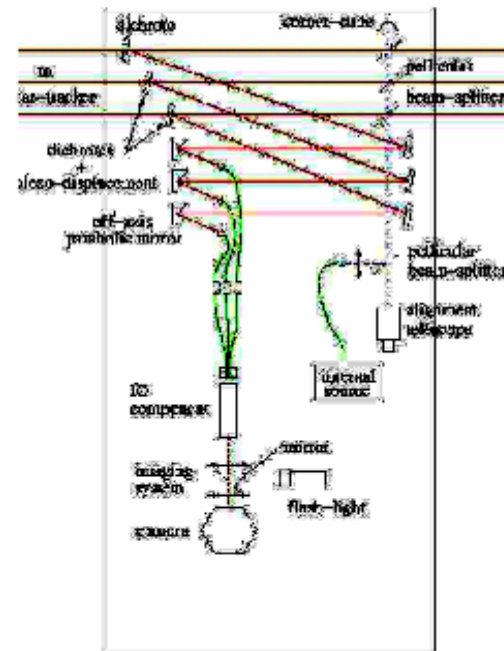


Figure 2. Schematic description of the IONIC bench (see text for details)

Integrated optics: 2

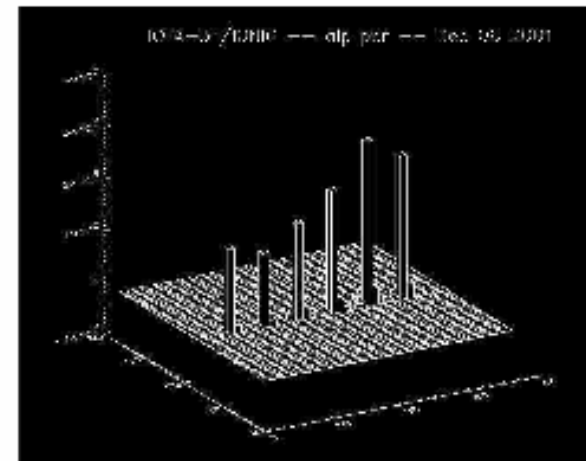
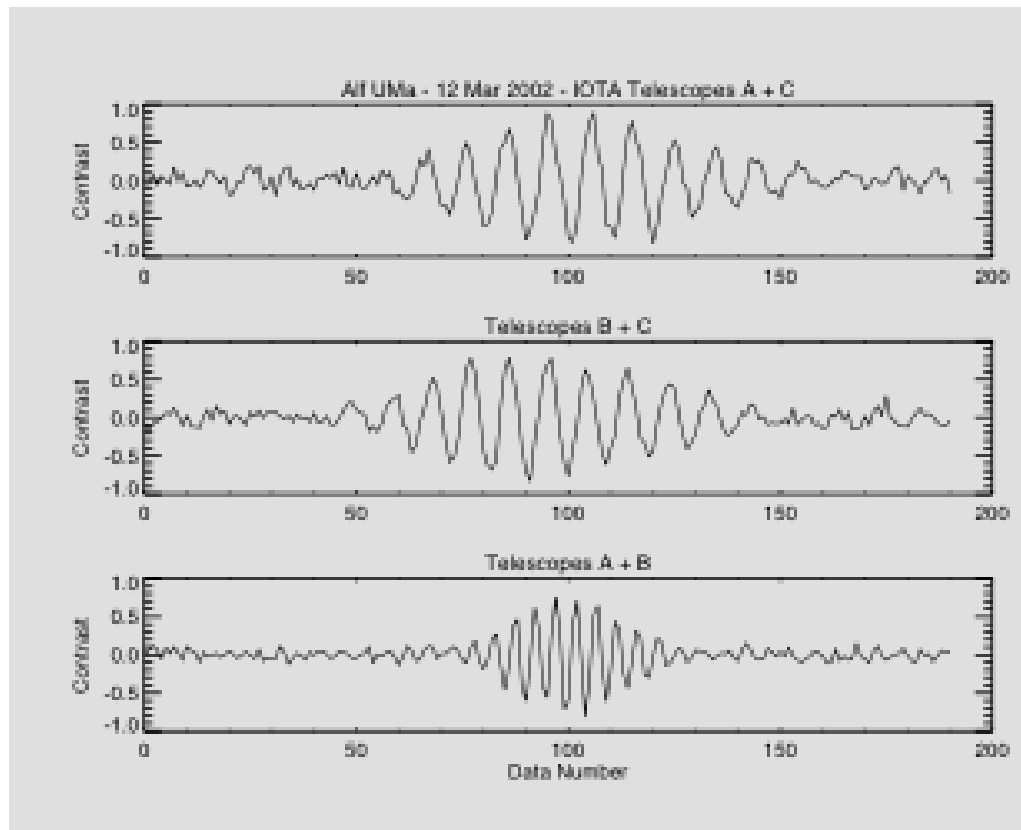
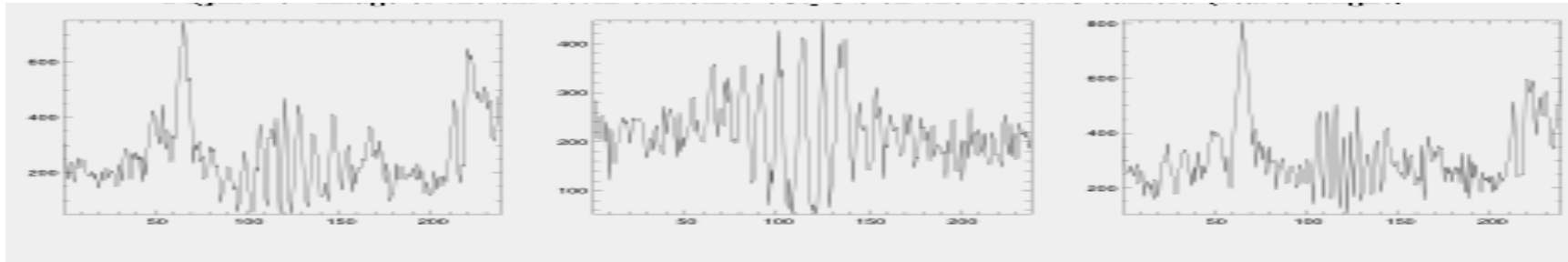
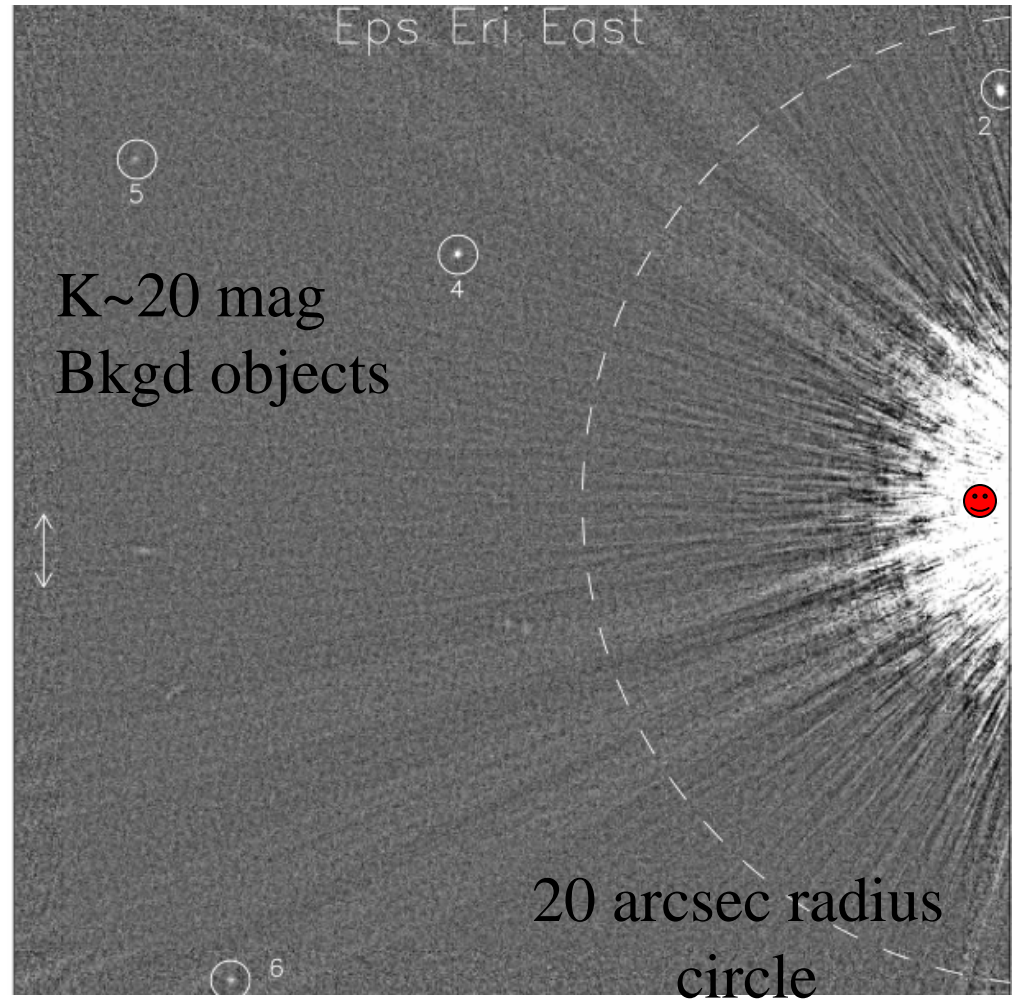
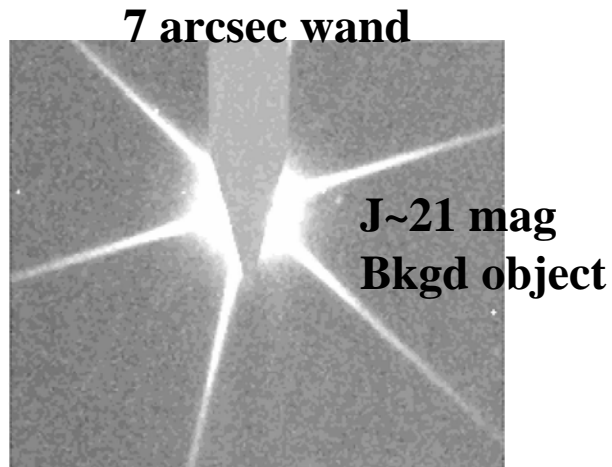
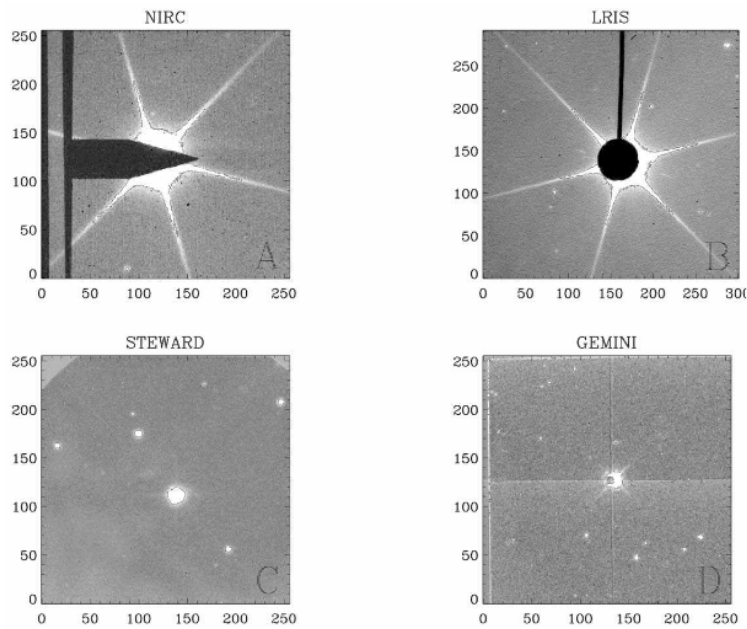


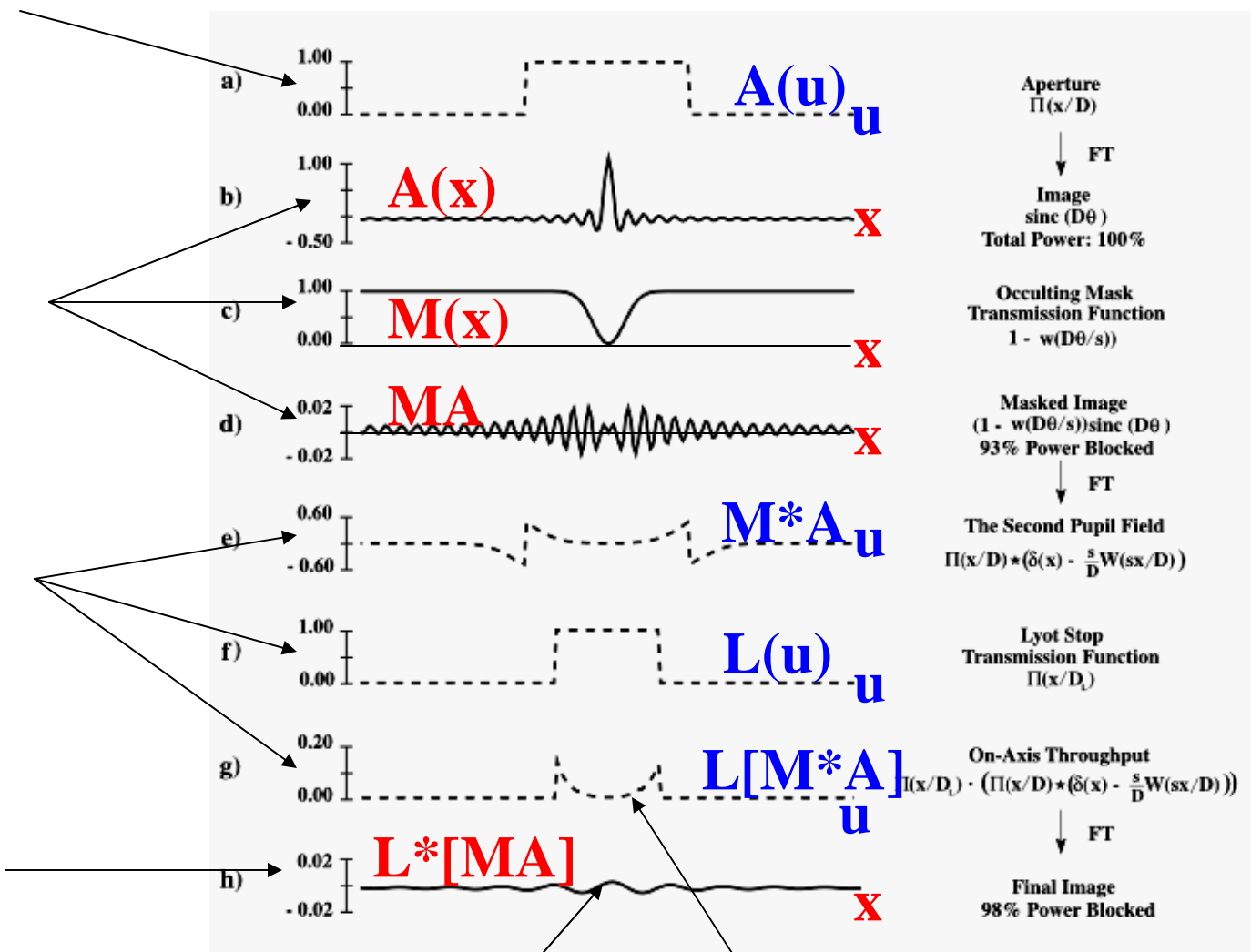
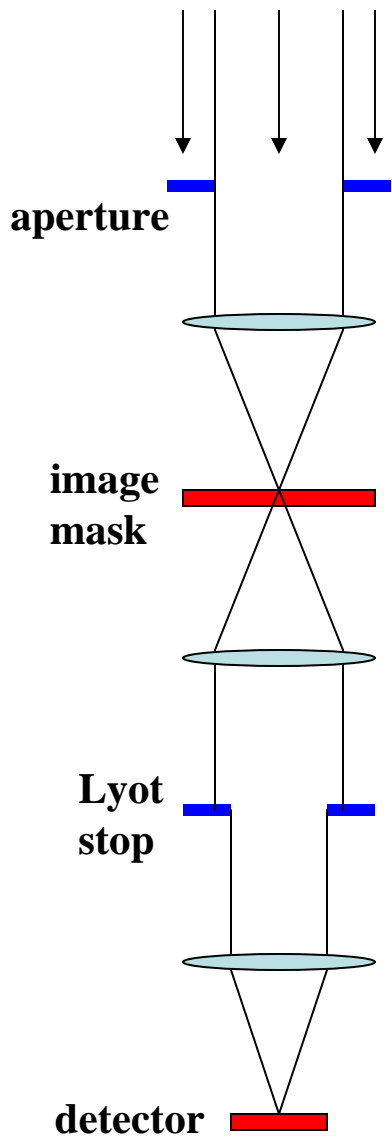
Image-plane Coronagraphs: a Very Quick Introduction

Current ground-based coronagraph examples



Ref: McCarthy & Zuckerman (2004); Macintosh et al (2003)

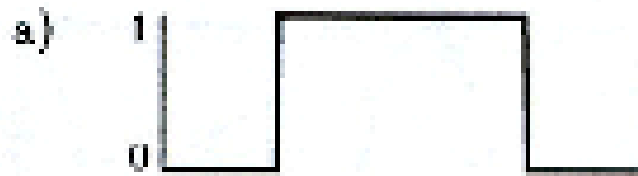
Classical Coronagraph



$$L(x) * [M(x) \cdot A(x)] \sim 0$$

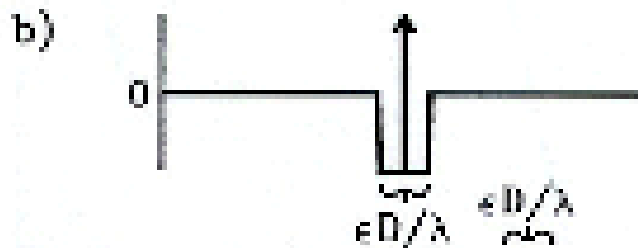
$$L(u) \cdot [M(u) * A(u)] \sim 0$$

Band-limited ($1 - \sin x/x$) mask



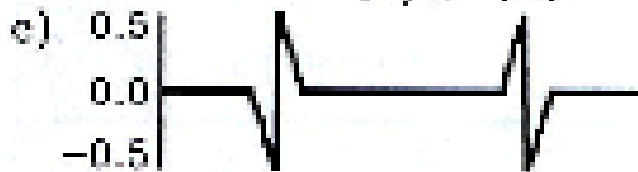
Aperture
 $A(u)$

Amplitude of
on-axis star = $1 e^{i0}$



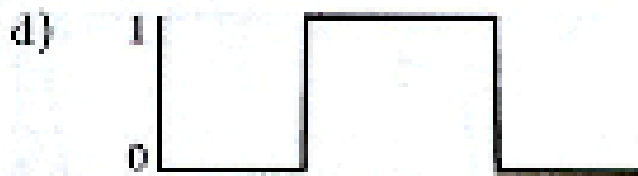
Conjugate of Mask ATF
 $M(u)$

**$FT(1 - \sin x/x) =$
 $\delta(u) + \text{rect}(u)$**



The Second Pupil Field
 $M(u) * A(u)$

Convolution



Lyot Stop
 $L(u)$

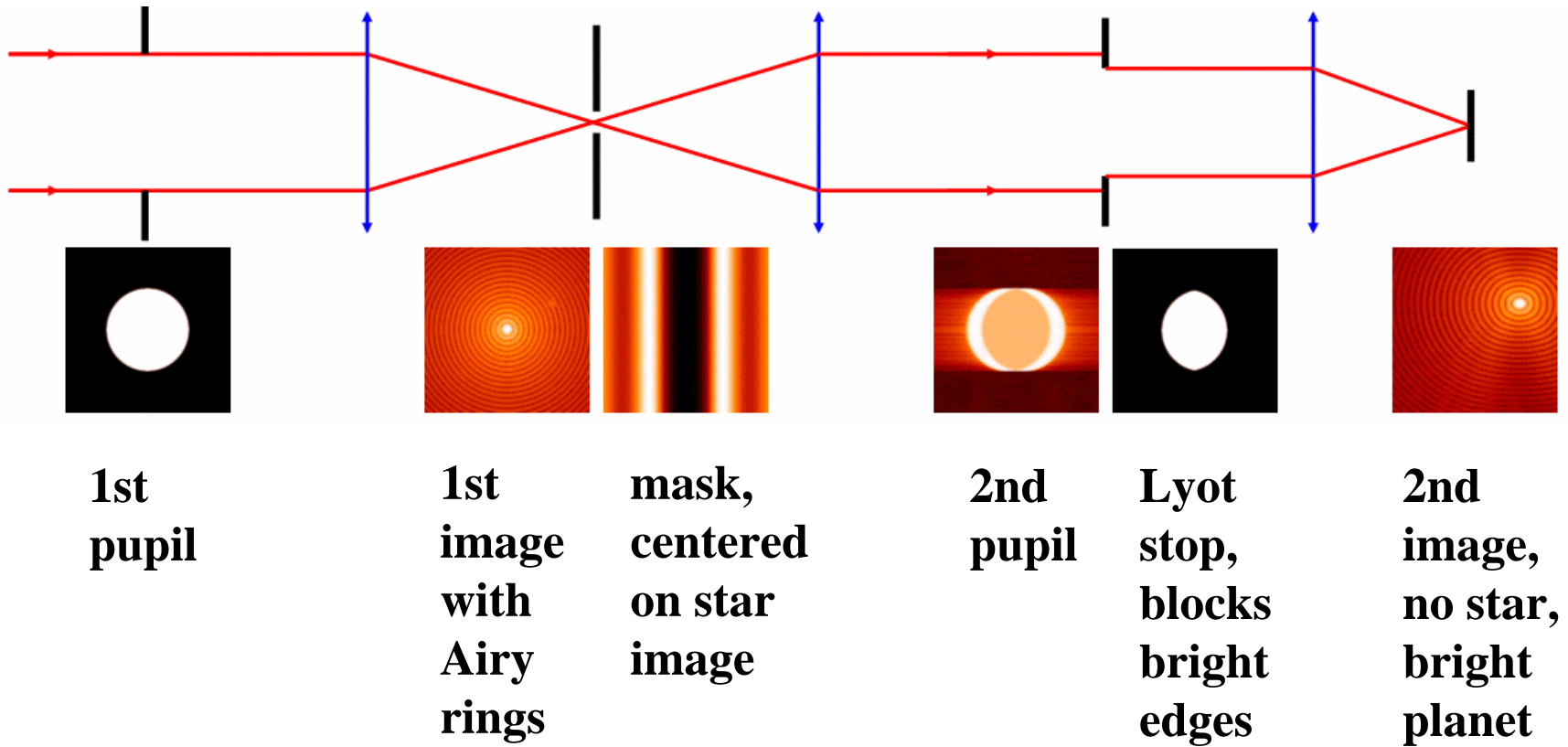
Lyot stop blocks
bright edges



The Final Field
 $L(u) (M(u) * A(u))$

Zero transmission
of on-axis star

Image-plane coronagraph simulation



Ref.: Pascal Borde 2004

Perturbation #1: ripples and speckles

Phase ripple and speckles

Suppose there is height error $h(u)$ across the pupil, where

$$h(u) = \sum_n a_n \cos(2\pi nu/D) + b_n \sin(2\pi nu/D) = \text{ripple}$$

The amplitude across the pupil is then

$$A(u) = e^{ikh(u)} \approx 1 + ik[\sum_n a_n \cos(2\pi nu/D) + b_n \sin(2\pi nu/D)]$$

In the image plane at angle α the amplitude will be

$$\begin{aligned} \mathbf{A}(\alpha) &= \int \mathbf{A}(u) e^{ik\alpha u} du \\ &= \delta(\mathbf{0}) + (i/2) \sum_n [(a_n - ib_n)\delta(k\alpha - \mathbf{K}n) + (a_n + ib_n)\delta(k\alpha + \mathbf{K}n)] \end{aligned}$$

where we use $\mathbf{K} = 2\pi/D$. The image intensity is then

$$\begin{aligned} \mathbf{I}(\alpha) &= \delta(\mathbf{0}) + (1/4) \sum_n (a_n^2 + b_n^2) [\delta(k\alpha - \mathbf{K}n) + \delta(k\alpha + \mathbf{K}n)] = \text{speckles} \\ &\text{at } \alpha = \pm n\lambda/D \end{aligned}$$

If we add a deformable mirror (DM), then $a_n \rightarrow a_n + A_n$ and $b_n \rightarrow b_n + B_n$

Commanding $A_n = -a_n$ and $B_n = -b_n$ forces all speckles to zero.

Phase + amplitude ripple and speckles

Suppose the height error $h(u)$ across the pupil is **complex**, where

$$h(u) = \sum_n (a_n + ia_n') \cos(Knu) + (b_n + ib_n') \sin(Knu) = \text{ripple}$$

i.e., we have both **phase and amplitude** ripples (= errors).

The image intensity is then

$$I(\alpha) = \delta(0) + (1/4) \sum_n [(a_n + b_n')^2 + (b_n - a_n')^2] \delta(k\alpha + Kn) \\ + [(a_n - b_n')^2 + (b_n + a_n')^2] \delta(k\alpha - Kn) = \text{speckles}$$

If we add a deformable mirror (DM), and command

$$A_n = -(a_n - b_n') \text{ and } B_n = -(b_n + a_n')$$

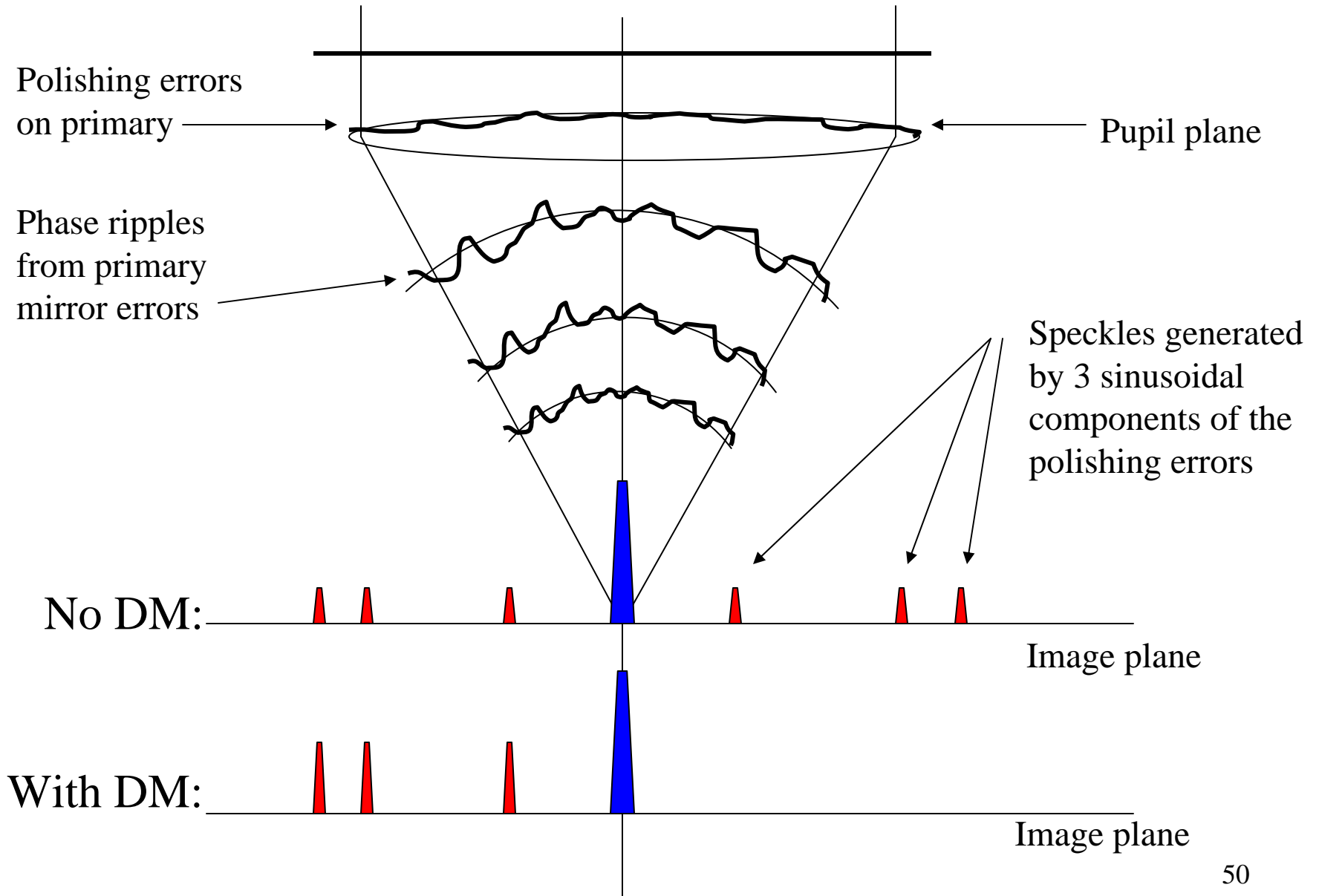
Then we get

$$I(\alpha) = \delta(0) + \sum_n [(b_n')^2 + (a_n')^2] \delta(k\alpha + Kn) \leftarrow \text{bigger speckles} \\ + [\mathbf{0} + \mathbf{0}] \delta(k\alpha - Kn) \leftarrow \text{smaller (zero) speckles}$$

So in **half the field of view** we get **no speckles**,

but in the other half we get stronger speckles.

Phase ripple and speckles



So, we discussed these topics:

1. Thinking in terms of wavelets.
2. Calculating the interference of wavefronts for any optical system.
3. Learning about astrophysical vs instrumental effects.
4. A teaser about coronagraphs and speckles.