

Wavefront Sensing & Control

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Slides based on material by Claire Max,
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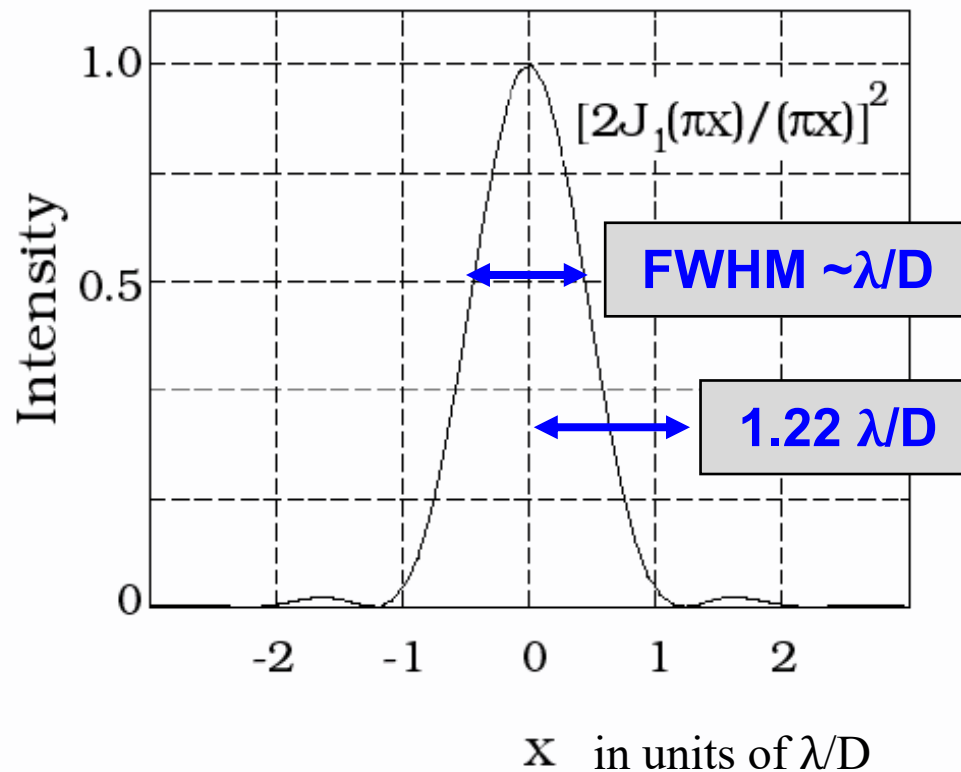






Imaging through a perfect telescope

Point Spread Function (PSF):
intensity profile from point source



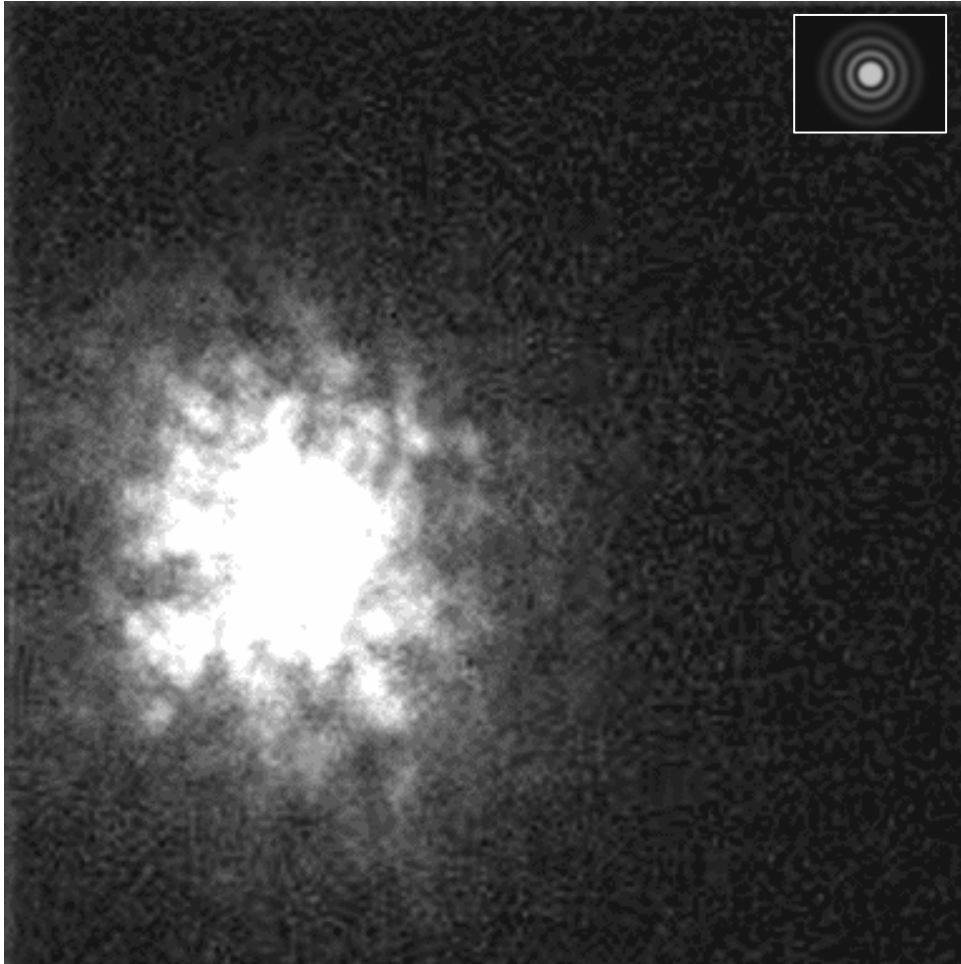
- With no turbulence, FWHM is the diffraction limit of telescope, $\theta \sim \lambda / D$
- With turbulence, the image size is much larger, typically 0.5 - 2 arcseconds





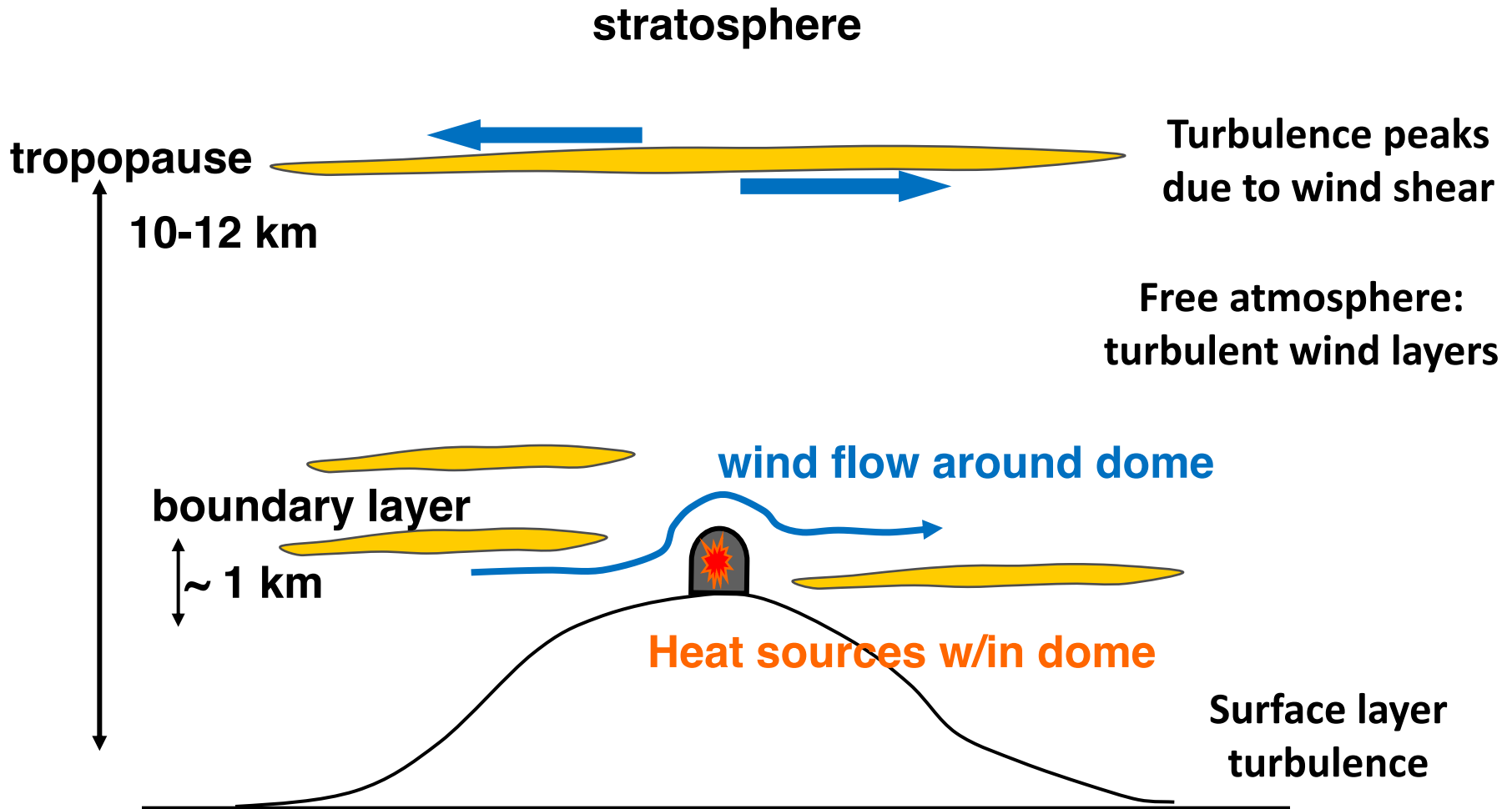


Turbulence changes rapidly with time

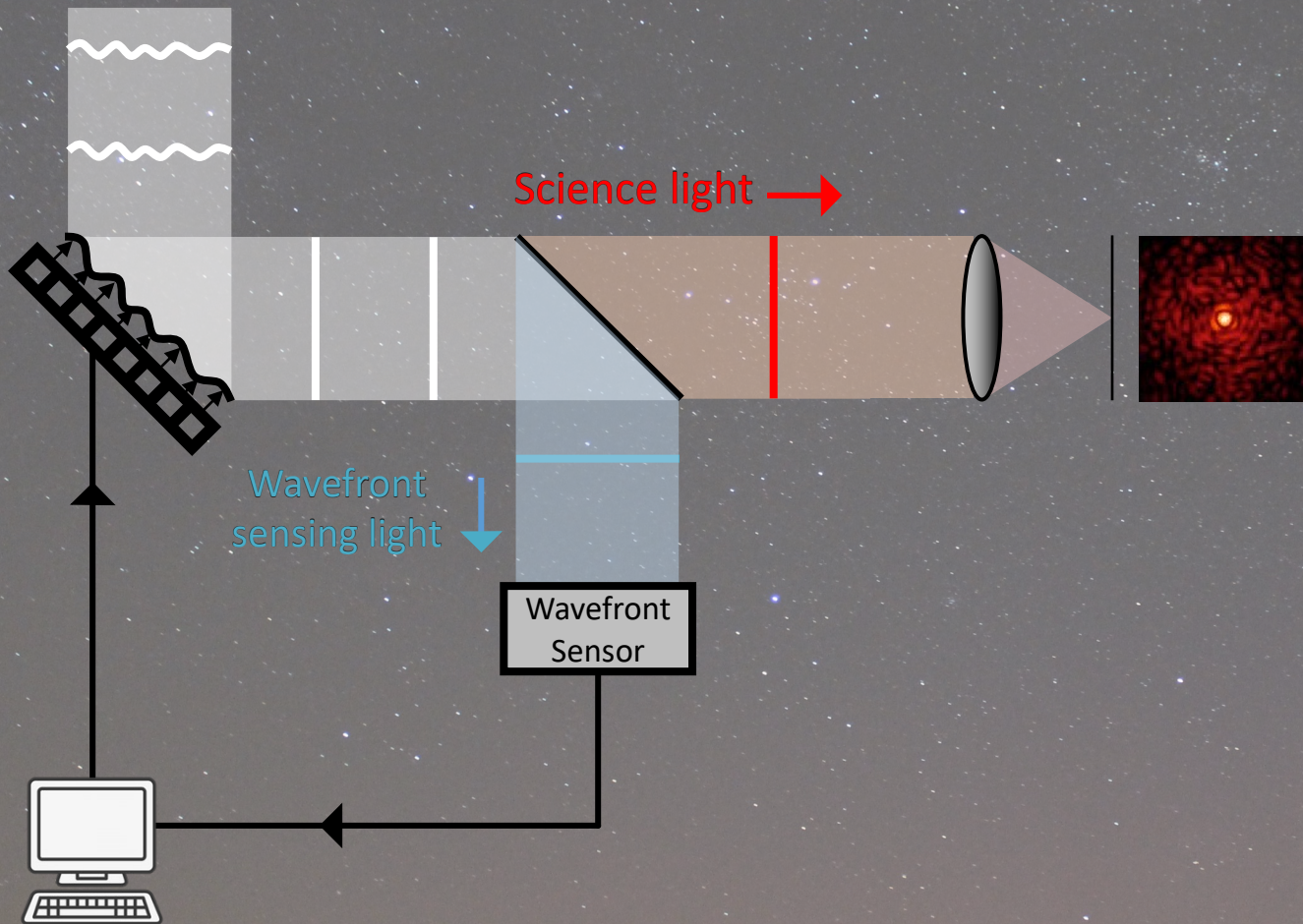


- Resulting images are a combination of many Airy discs at different locations, called speckles
- Each Airy disc is defined by the diffraction limit of the telescope
- Centroid jumps around (image motion)

Turbulence arises at many locations



Cartoon Diagram of an Adaptive Optics System



An idealized deformable mirror

BEFORE

AFTER



**Incoming
Wave with
Aberration**

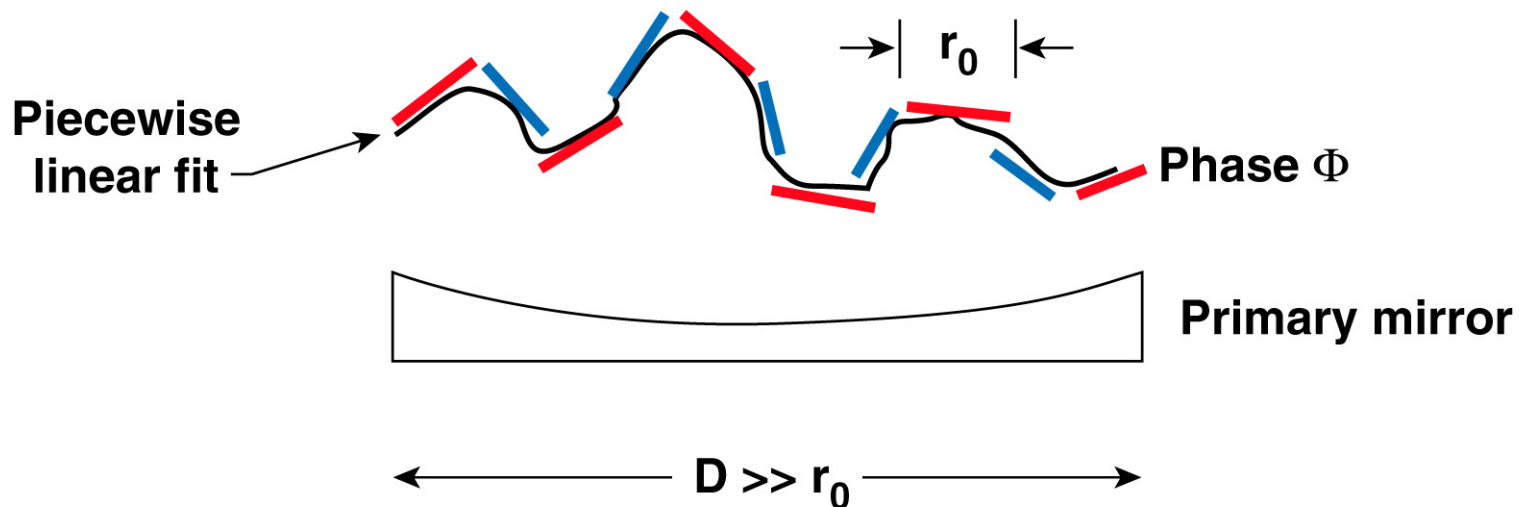
**Deformable
Mirror**

**Corrected
Wavefront**

Deformable mirror requirements: r_0 sets the required # of degrees of freedom

- The spatial scale of turbulence is described by the Fried parameter, r_0

$$r_0 \equiv \left[0.423 k^2 (\sec z) \int C_N^2 dh \right]^{-3/5}$$



- Number of subapertures is approximately $(D/r_0)^2$ where r_0 is evaluated at the desired observing wavelength

DM Requirements

- **Dynamic Range:** from turbulence theory, the variance across a wavefront is:

$$\sigma_{\text{wavefront}}^2 = 6.88(D/r_0)^{5/3} [\text{rad}^2]$$

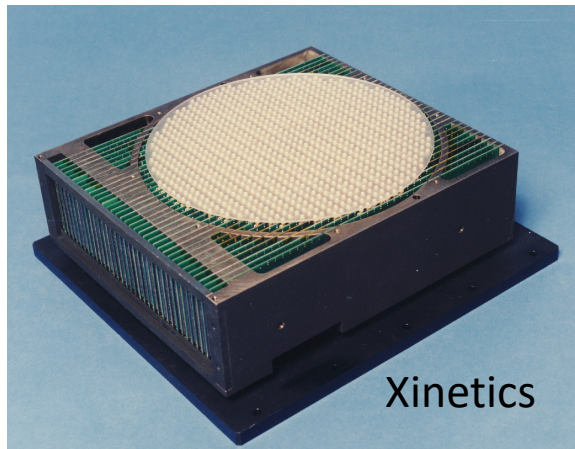
For Keck, $\sigma \sim 5.5$ microns

For ELTs, $\sigma \sim 30$ microns

- **Temporal Response:** should be much faster than the coherence time ($\sim 1\%$) to avoid limiting the system's performance (1-2ms in the NIR)
 - The temporal scale of the atmosphere is given by $\tau_0 \sim \left(\frac{r_0}{\bar{v}}\right)$
- **Influence Function:** a continuous facesheet DM needs a good match between the facesheet thickness and actuator spacing
- **Other requirements:** surface quality, actuator hysteresis, power dissipation, and size

Deformable mirrors come in many genres and sizes

Glass facesheet DM
1000 actuators

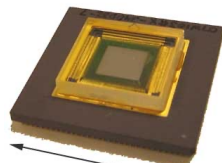


Xinetics

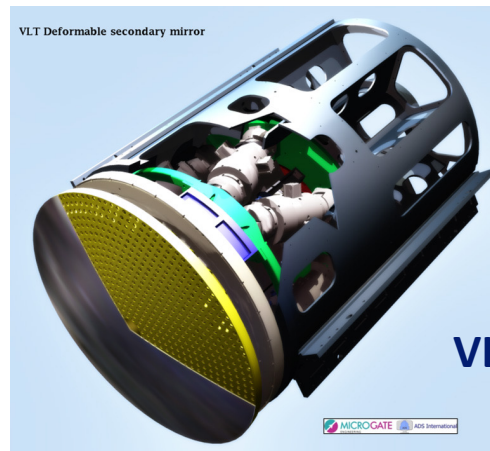


LBT adaptive secondary
672 actuators

Boston Micromachins MEMS DM
1000 actuators



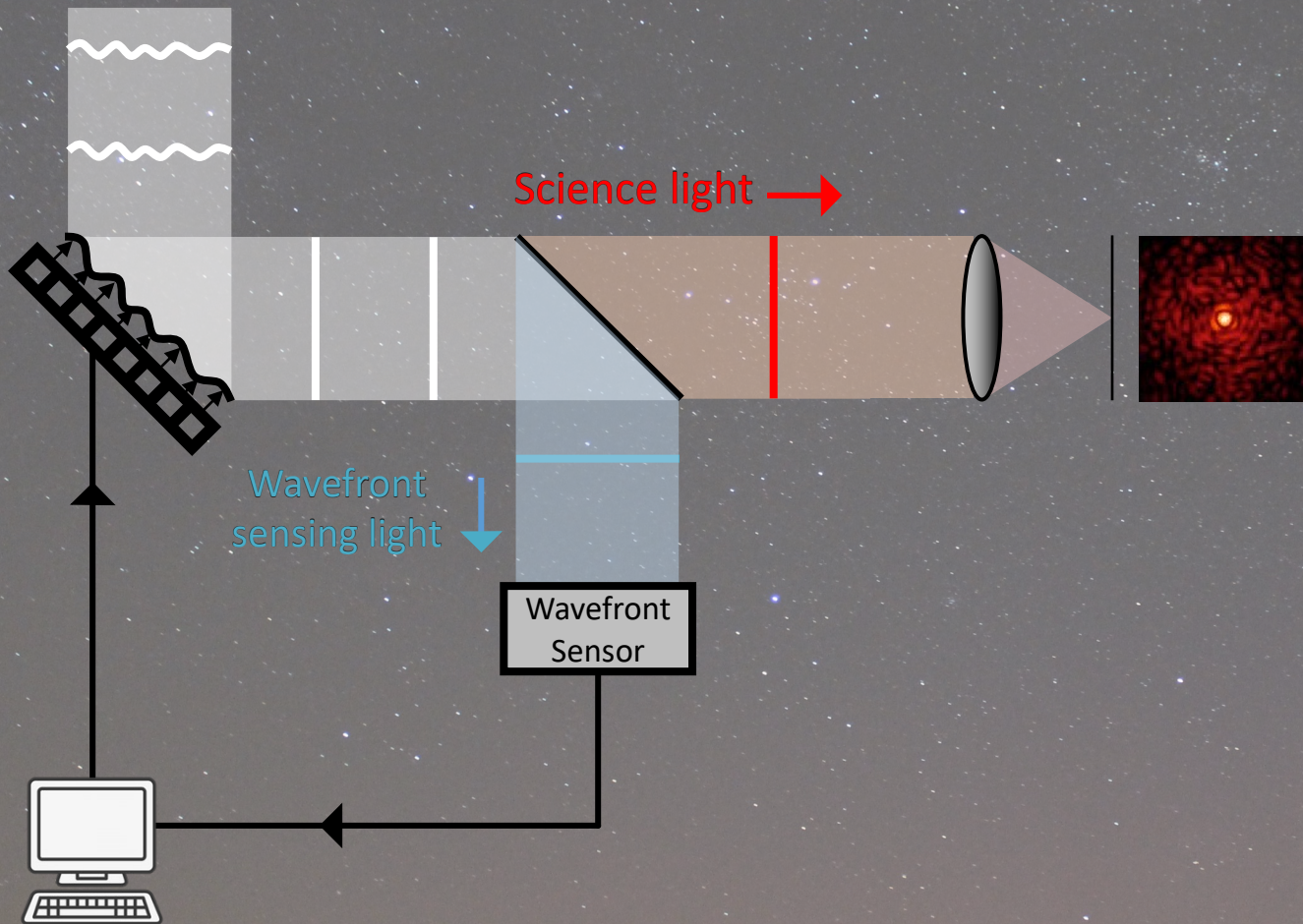
1 cm



VLT adaptive secondary

1170 actuators

Cartoon Diagram of an Adaptive Optics System



Wavefront Sensor Requirements

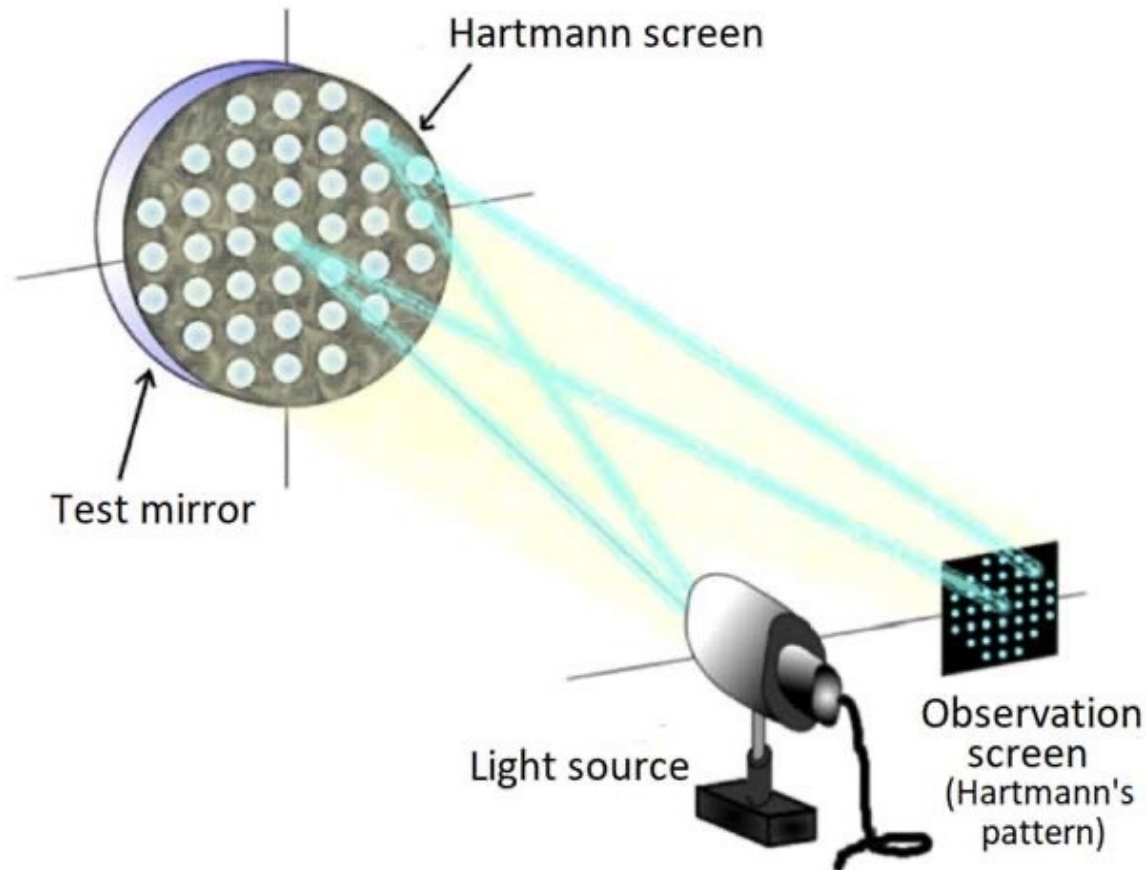
- **Spatial resolution:** should at least match what DM can correct
- **Dynamic range:** should be able to measure large amplitude aberrations
- **Sensitivity:** should be able to measure small amplitude aberrations
- **Temporal requirement:** AO loop needs to run on timescale of atmospheric turbulence (millisecond timescales)
- **Linear range:** linear relation between input phase variation and output intensity variation
- **Efficient use of photons:** allows for use of faint light sources
- Ability to work on both **point sources and extended sources**, operate over **wide range of wavelengths**

Types of Wavefront Sensors

- **Pupil plane:** wavefront properties are deduced by splitting the pupil into subapertures and measuring the intensity in each subaperture
 - Examples include Shack-Hartmann, Pyramid sensing
- **Focal plane:** wavefront properties are deduced from intensity measurements made at or near the focal plane.
 - Examples that are typically used to measure ~static aberrations:
 - Phase retrieval, e.g. Gerchberg-Saxton algorithm
 - Mostly iterative with long computation times compared to pupil plane
 - Examples that measure residual atmospheric aberrations as well:
 - Self-coherent camera

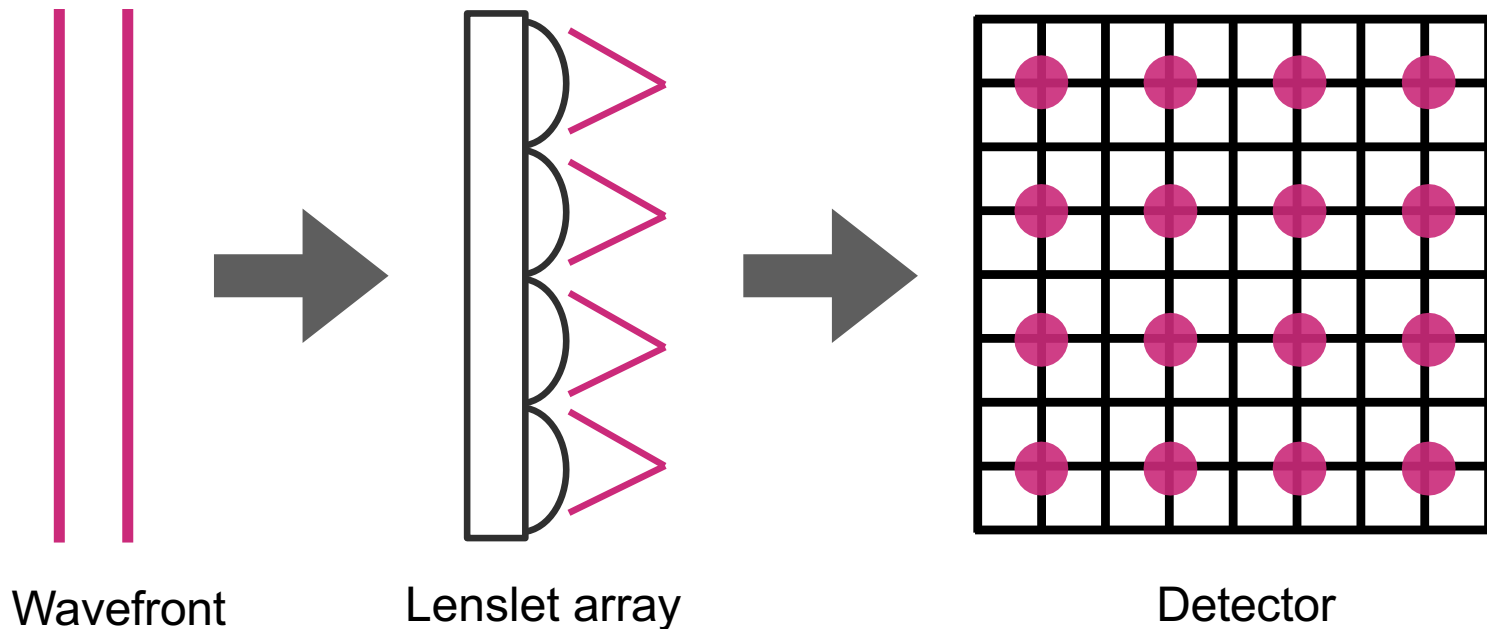
The Shack-Hartmann Wavefront Sensor

- Johannes Hartmann (1904): grid of holes mask placed to observe resulting dot pattern

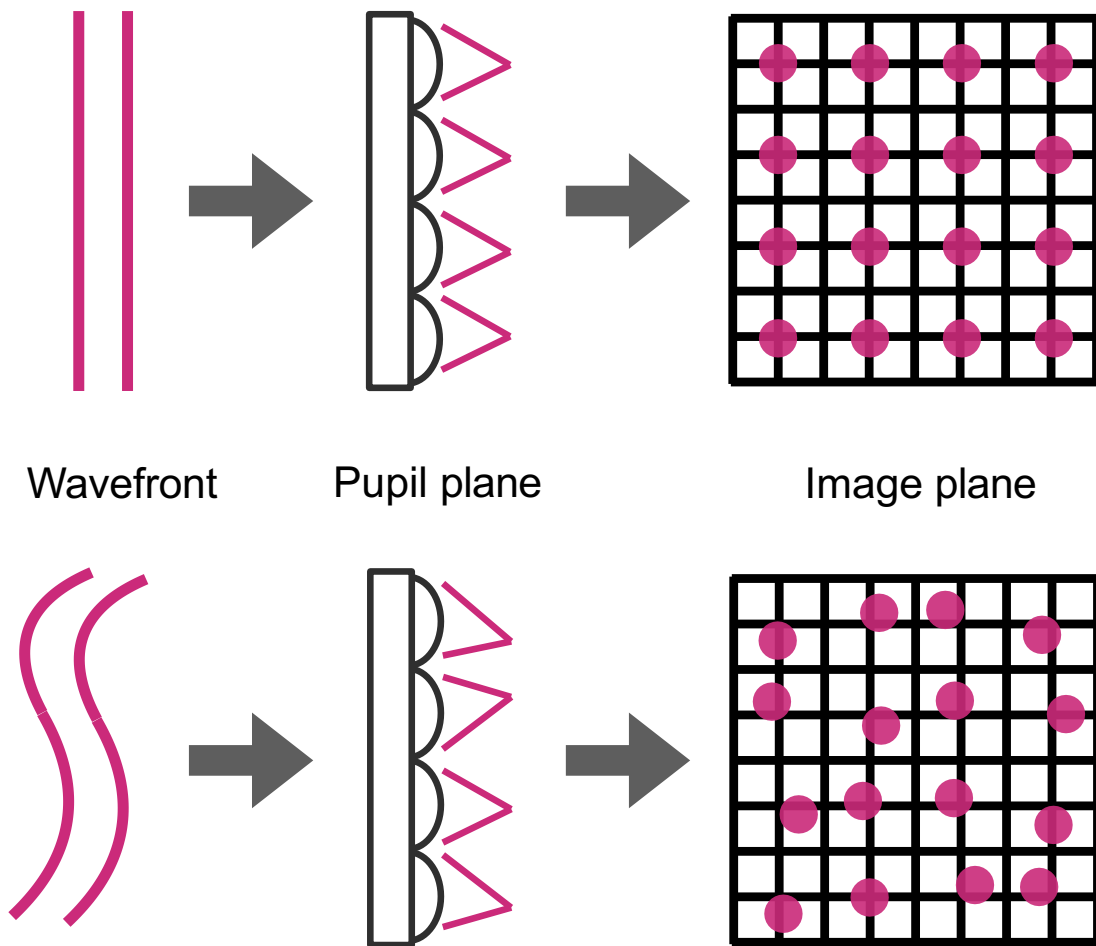


The Shack-Hartmann Wavefront Sensor

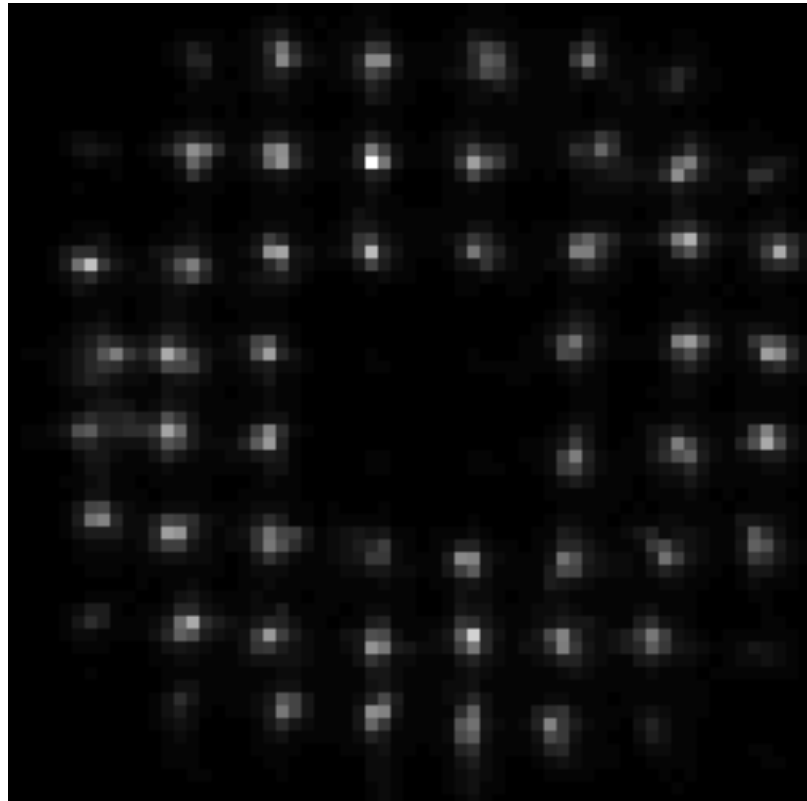
- Johannes Hartmann (1904): grid of holes mask placed to observe resulting dot pattern
- Roland Shack (1970s): replace holes with an array of lenses to improve light efficiency



The Shack-Hartmann Wavefront Sensor

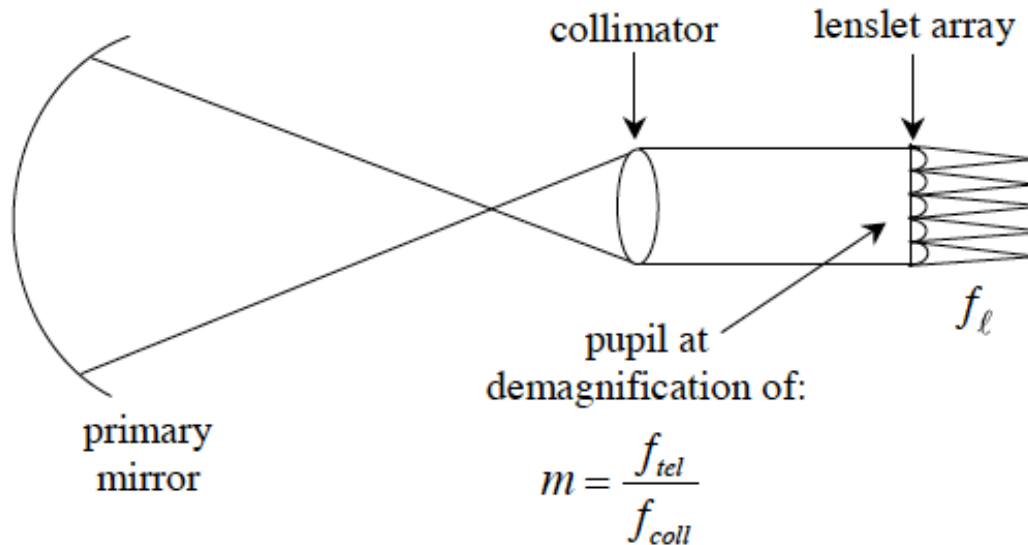


Example: Shack-Hartmann Wavefront Signals



Credit: Cyril Cavadore

Quantitative description of Shack-Hartmann operation

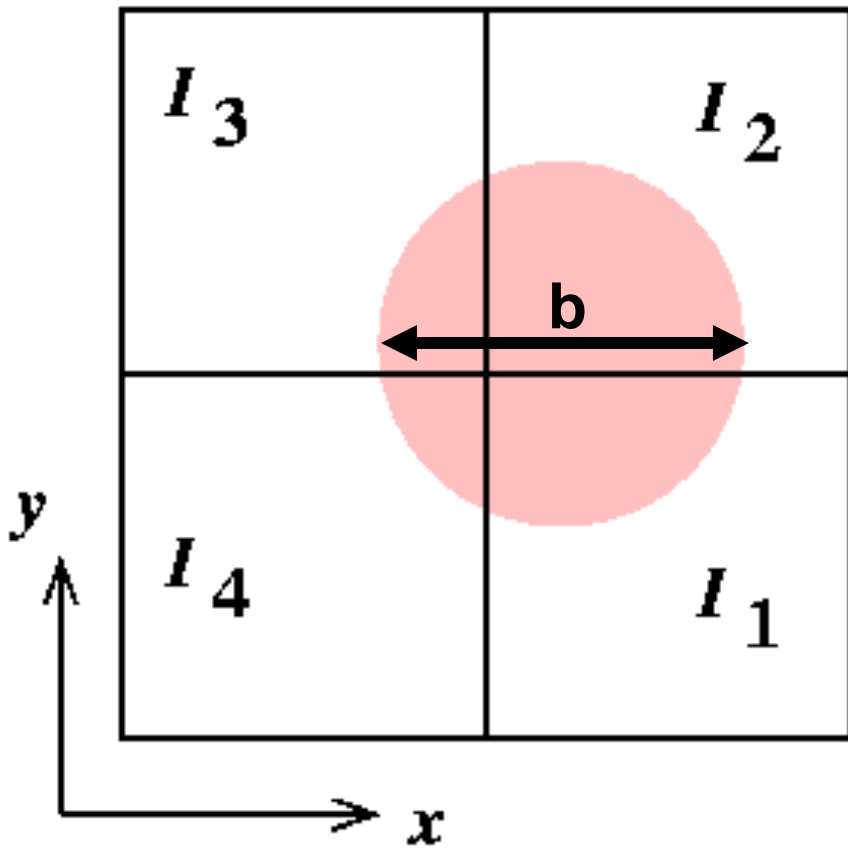


- The relationship between the displacement of Shack-Hartmann spots and the slope of wavefront:

$$k\Delta x = Mf\nabla\phi(x, y)$$

where $k = 2\pi / \lambda$, Δx is the lateral displacement of a subaperture image, M is the magnification of the system, f is the focal length of the lenslets in front of the Shack-Hartmann sensor

How do we measure $\Delta\vec{x}$: the distance a spot has moved on the detector? “Quad cell formula”

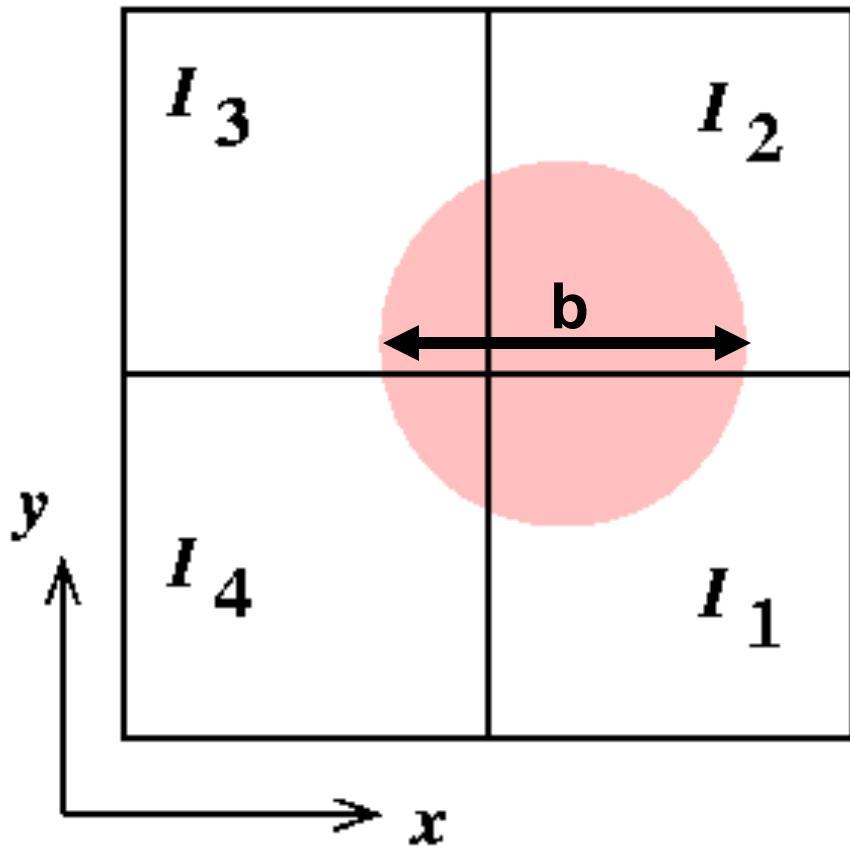


$$\delta_x \cong \frac{b}{2} \left[\frac{(I_2 + I_1) - (I_3 + I_4)}{(I_1 + I_2 + I_3 + I_4)} \right]$$

$$\delta_y \cong \frac{b}{2} \left[\frac{(I_3 + I_2) - (I_4 + I_1)}{(I_1 + I_2 + I_3 + I_4)} \right]$$

$$\delta_{x,y} = \frac{b (\text{difference of } I \text{'s})}{2 (\text{sum of } I \text{'s})}$$

How do we measure $\Delta \vec{x}$: the distance a spot has moved on the detector? “Quad cell formula”



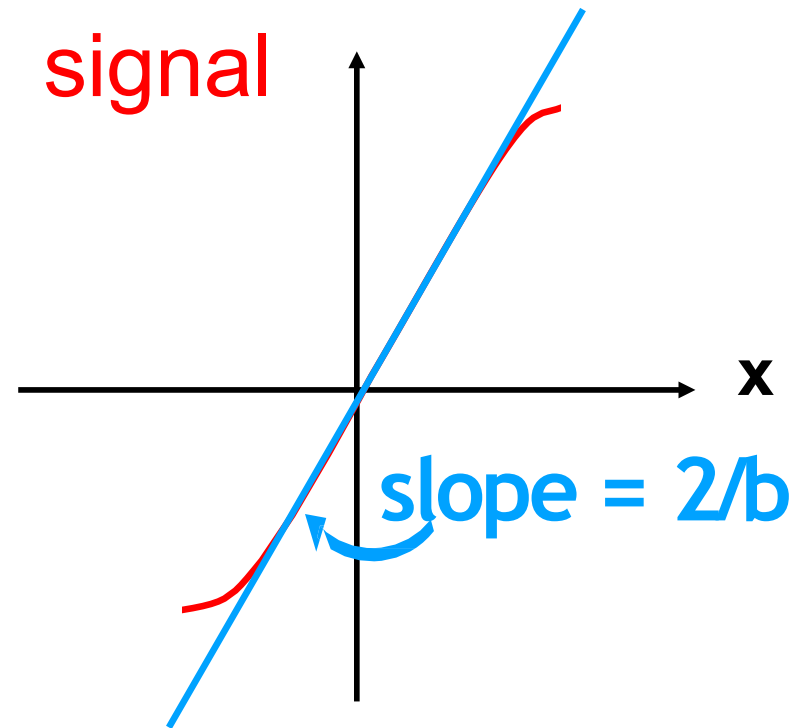
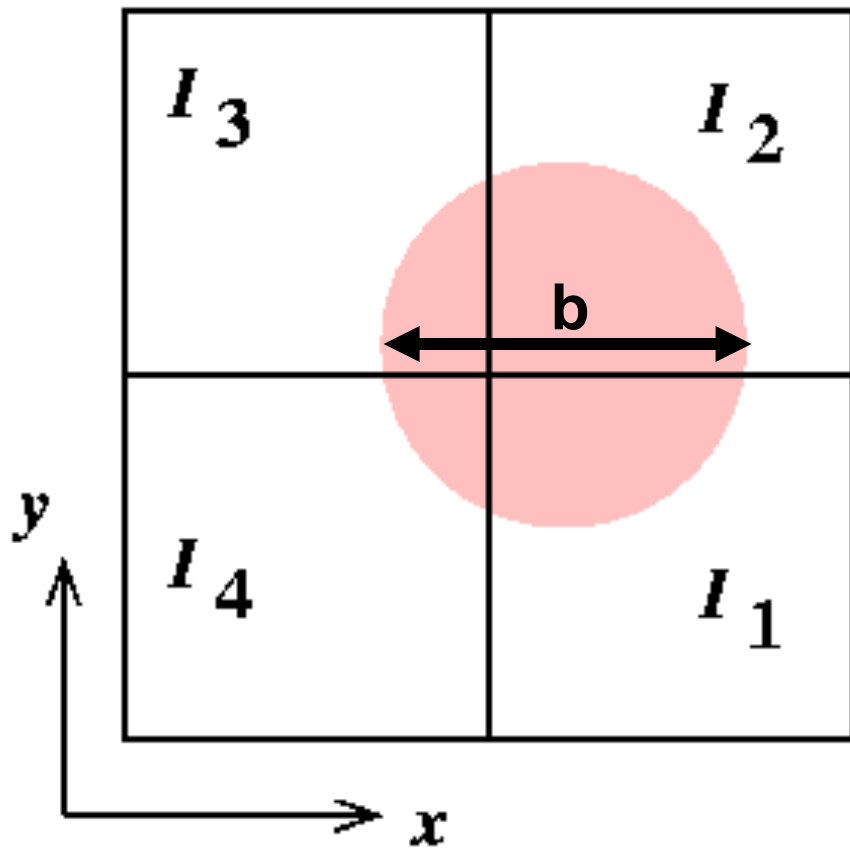
“Signal” in x

$$\delta_x \cong \frac{b}{2} \left[\frac{(I_2 + I_1) - (I_3 + I_4)}{(I_1 + I_2 + I_3 + I_4)} \right]$$

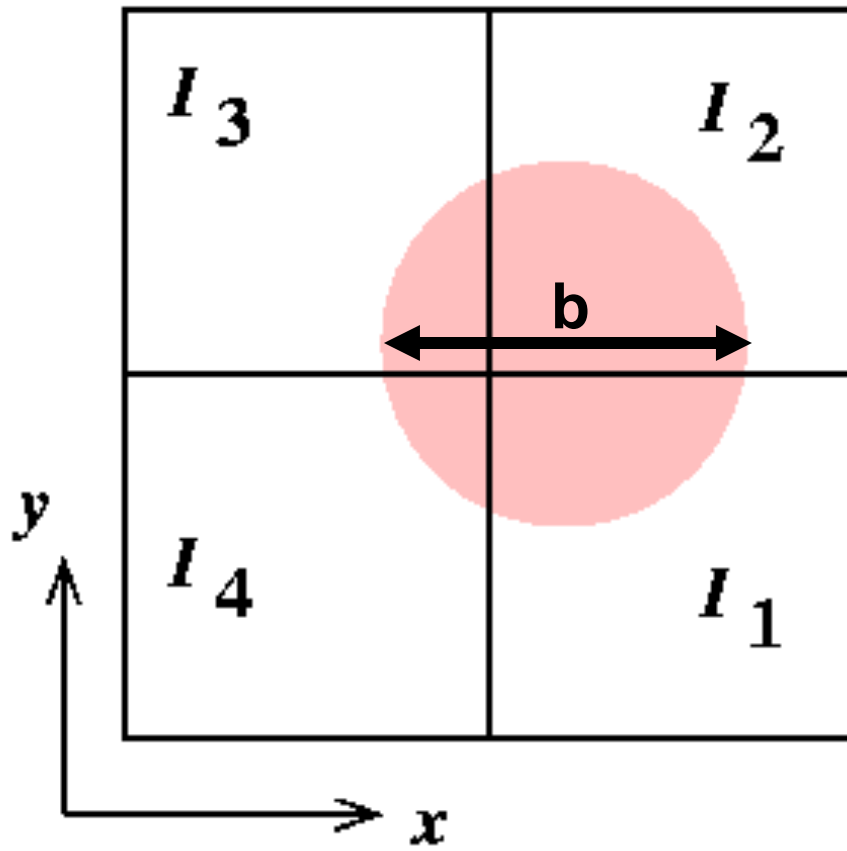
$$\delta_y \cong \frac{b}{2} \left[\frac{(I_3 + I_2) - (I_4 + I_1)}{(I_1 + I_2 + I_3 + I_4)} \right]$$

$$\delta_{x,y} = \frac{b (\text{difference of } I \text{'s})}{2 (\text{sum of } I \text{'s})}$$

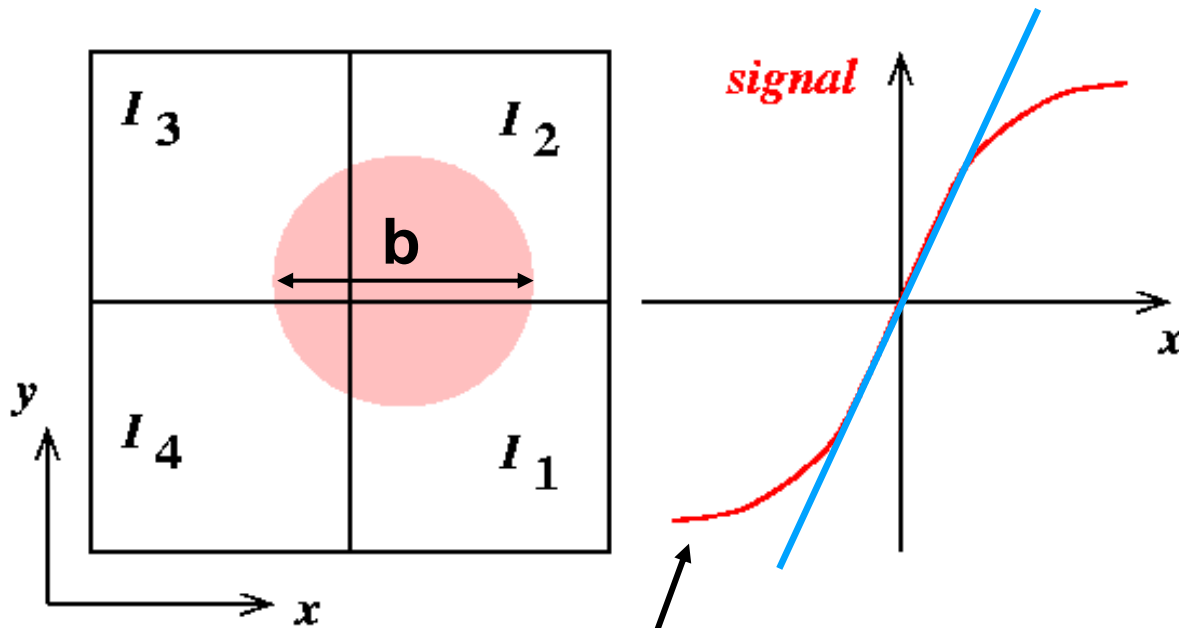
How do we measure the distance a spot has moved on the CCD? “Quad cell formula”



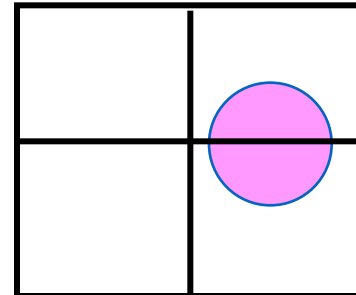
Concept Question: What might happen if the displacement of the spot is $>$ radius of spot?



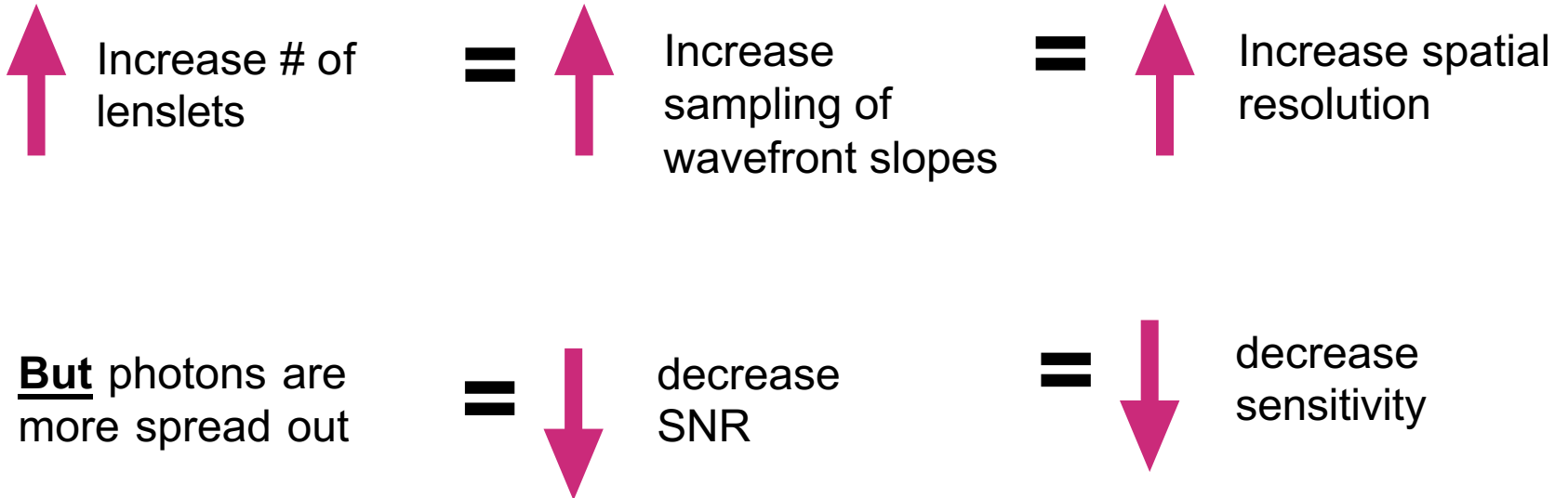
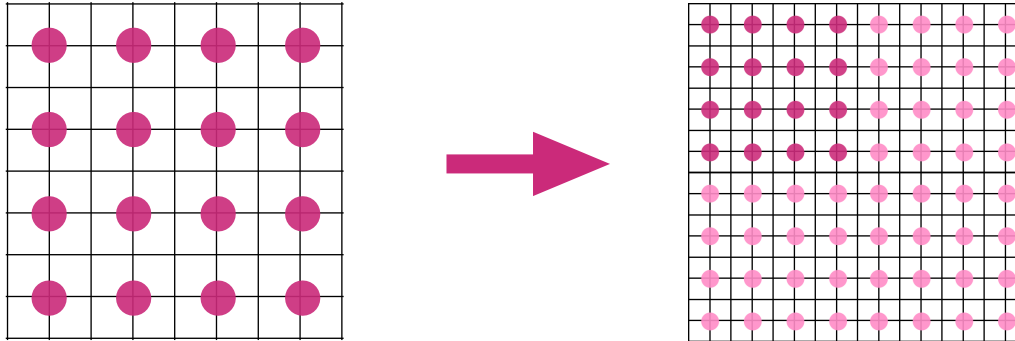
Signal becomes nonlinear and saturates for large angular deviations



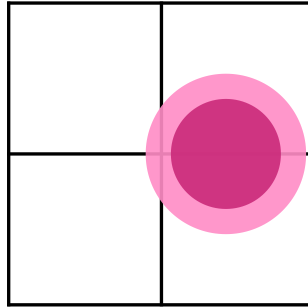
“Rollover” corresponds to spot being entirely outside of 2 quadrants



SHWFS Sources of Error: # Lenslets



SHWFS Sources of Error: spot size relative to the subaperture size



↑ Increase spot size (e.g. defocus)

=

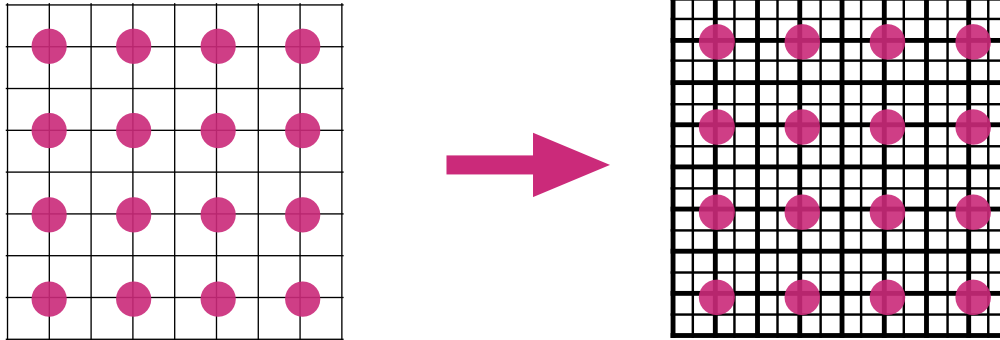
↑ Increase dynamic range

But less accurate centroiding

=

↓ decrease sensitivity

SHWFS Sources of Error: # of pixels



↑ Increase #
pixels

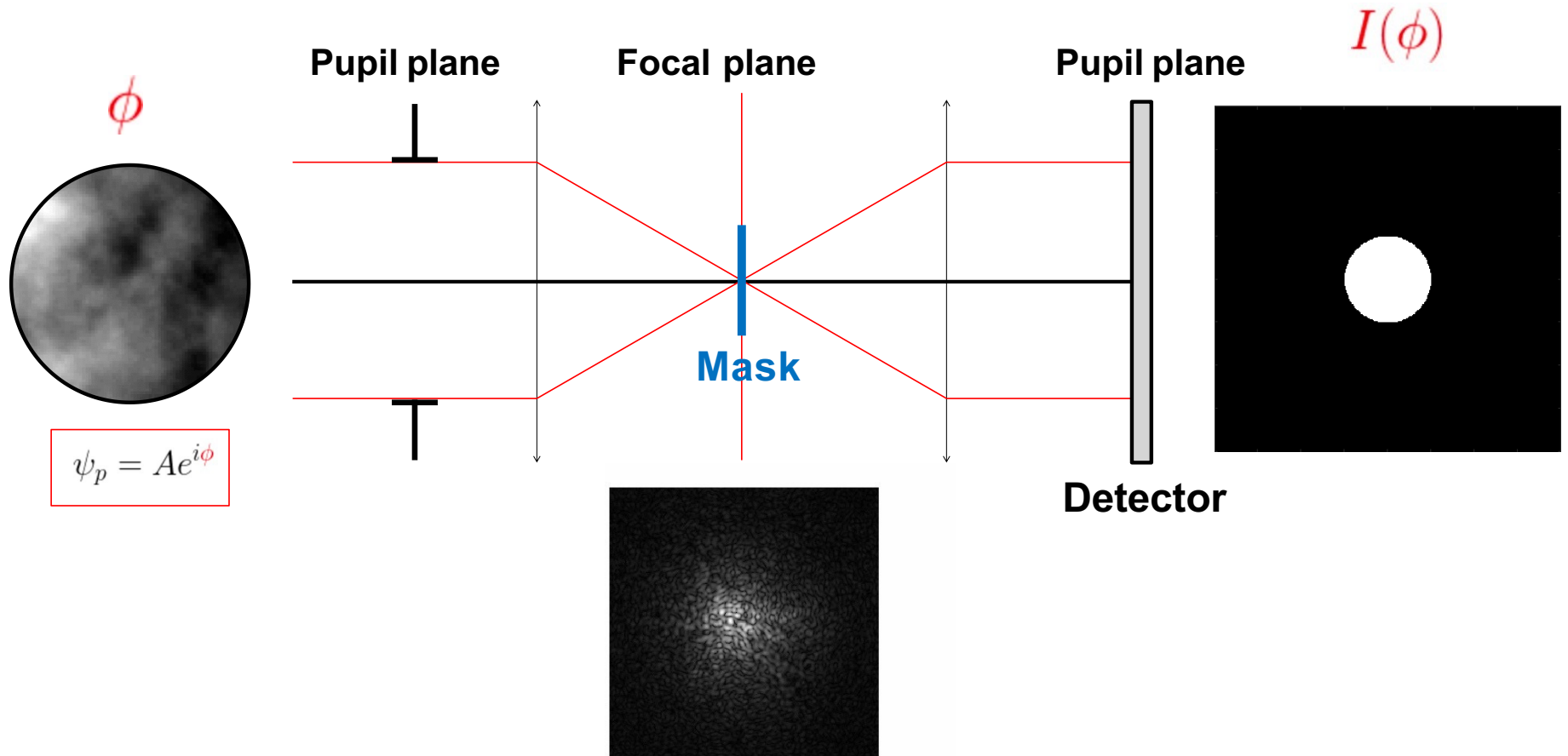
= ↑ Increase
centroiding
accuracy

(Measure position of spots by
estimating center of gravity
positions instead of quad-cell)

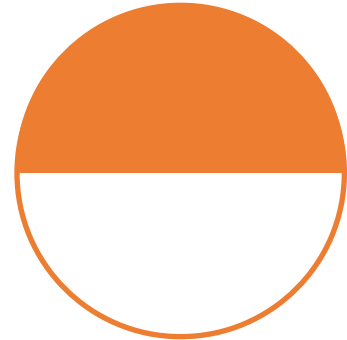
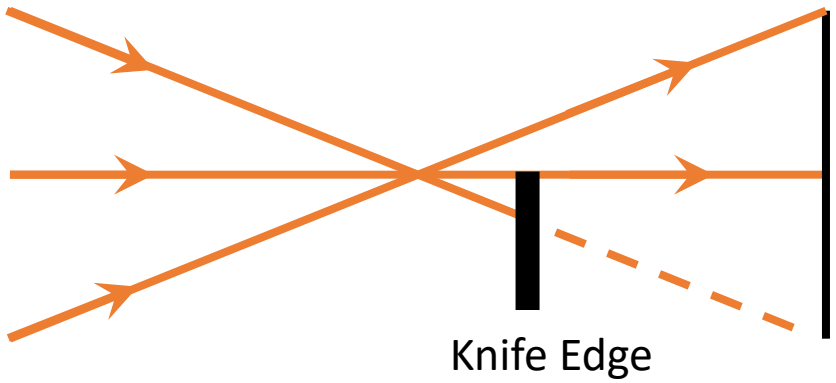
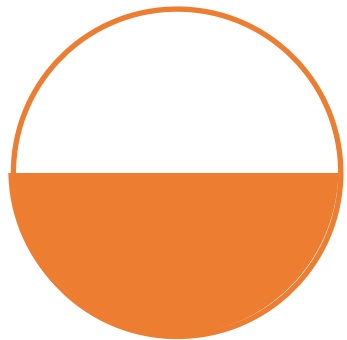
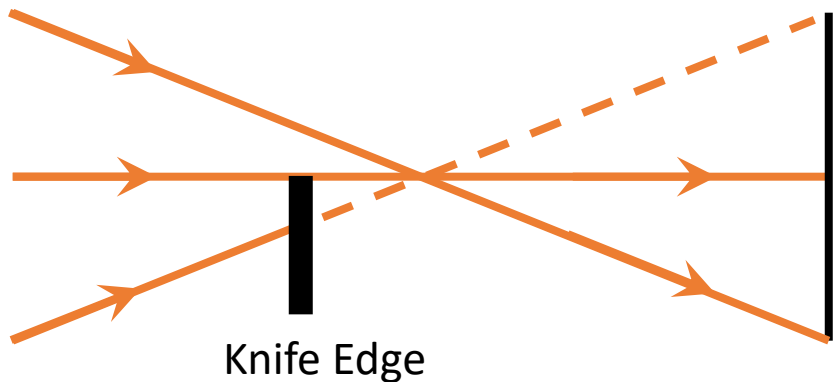
But photons are
spread out over
more pixels

= ↓ decrease
SNR

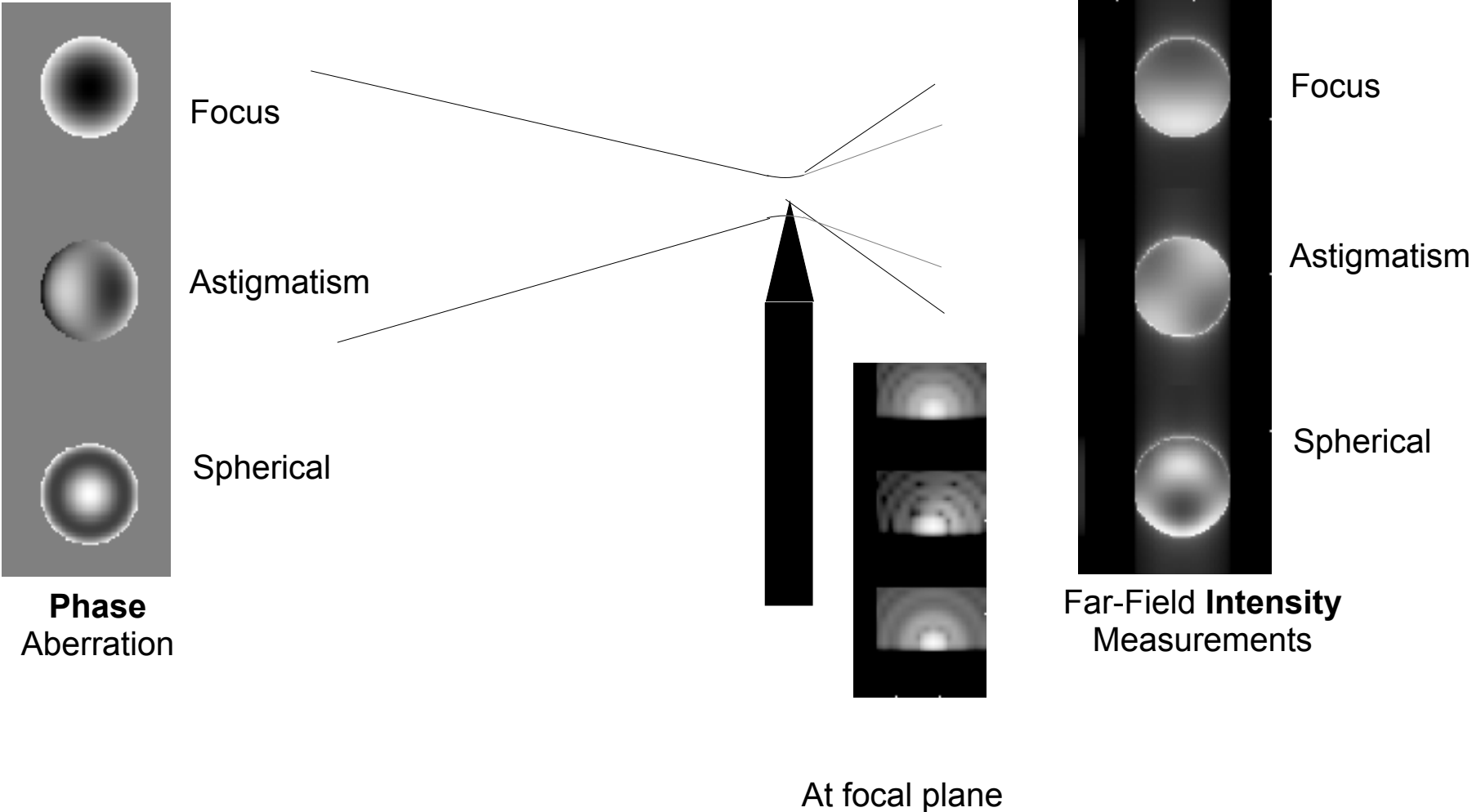
Fourier-Filtering Wavefront Sensors



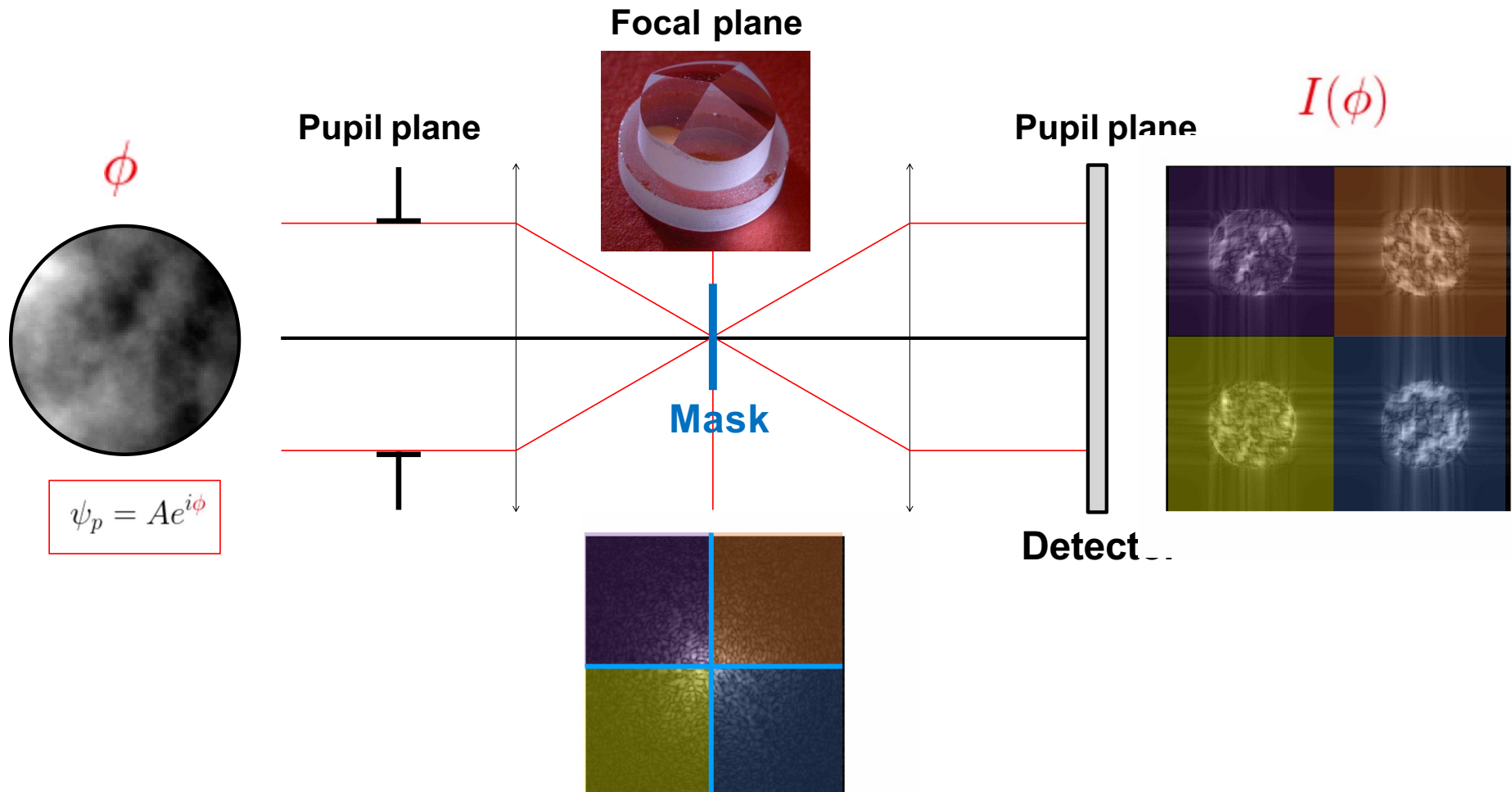
Foucault Knife Edge Test: an early example of a Fourier-filtering WFS



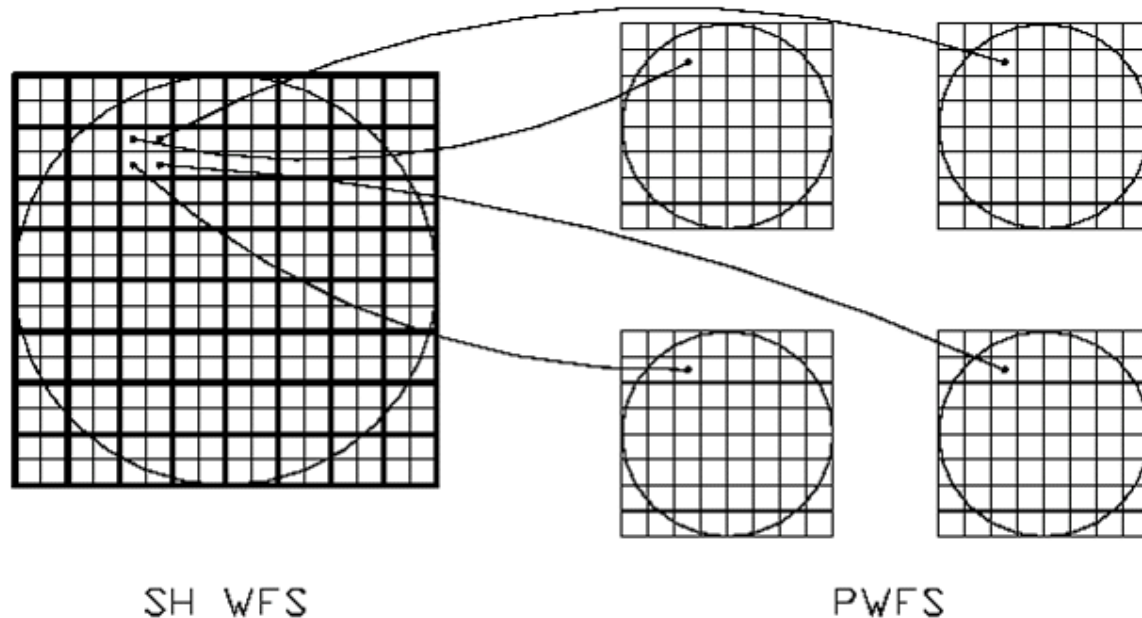
Fourier-filtering WFS: Foucault Knife Edge Test



Fourier-filtering WFS: Pyramid Wavefront Sensor (Ragazzoni 1996)



Pyramid sensor reverses order of operations in a Shack-Hartmann sensor

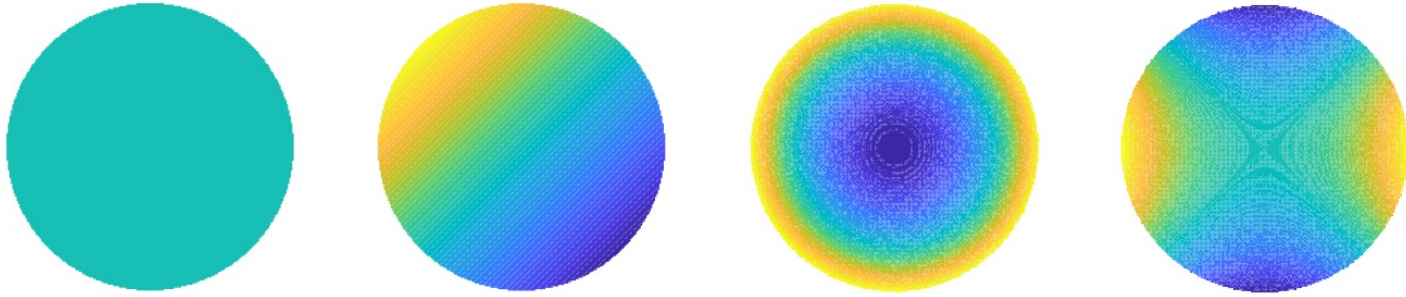


- Slope-like signal for each subaperture is given by:

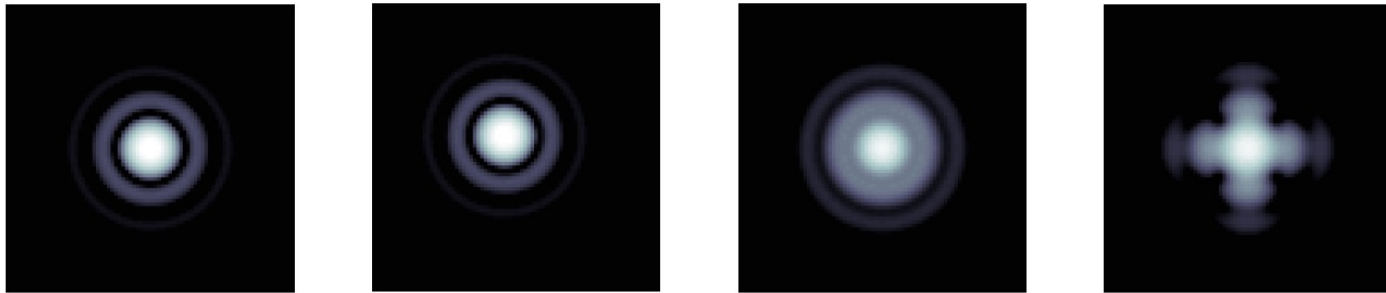
$$S_x(x, y) = [(I_1(x, y) + I_2(x, y)) - (I_3(x, y) + I_4(x, y))]/I_0,$$

$$S_y(x, y) = [(I_1(x, y) + I_4(x, y)) - (I_2(x, y) + I_3(x, y))]/I_0,$$

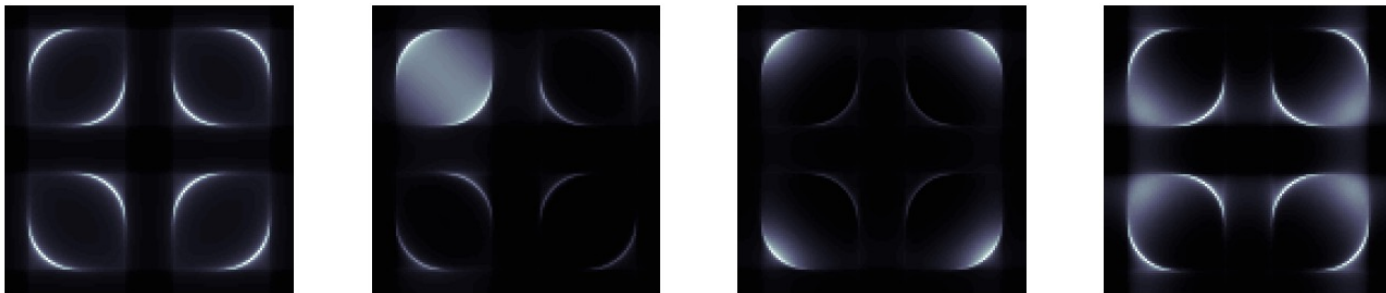
Typical intensity patterns for a Pyramid Sensor



(a) Low order wavefront aberrations.

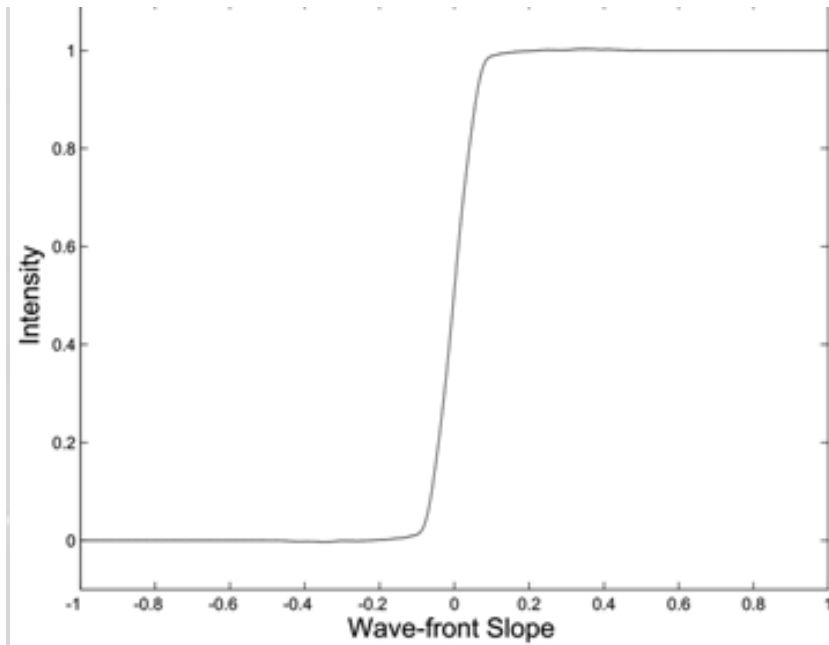
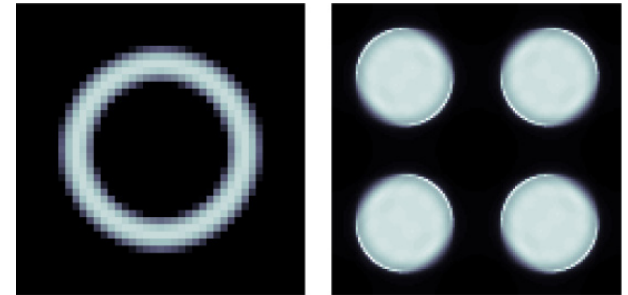
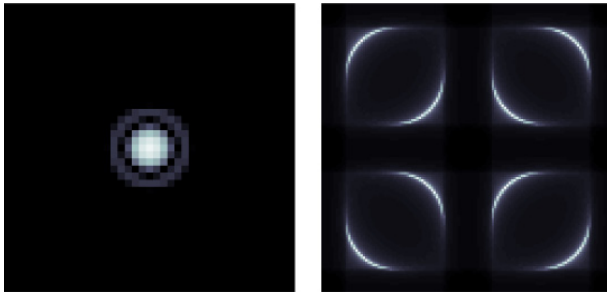


(b) Focal plane images for low order wavefront aberrations.

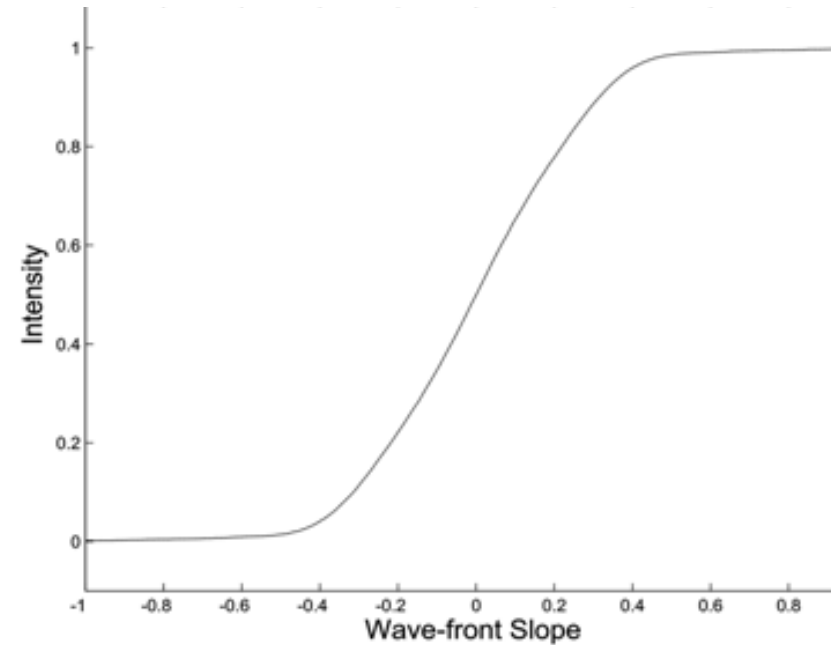


(c) Pyramid WFS signals for low order wavefront aberrations.

The Modulated Pyramid Wavefront Sensor

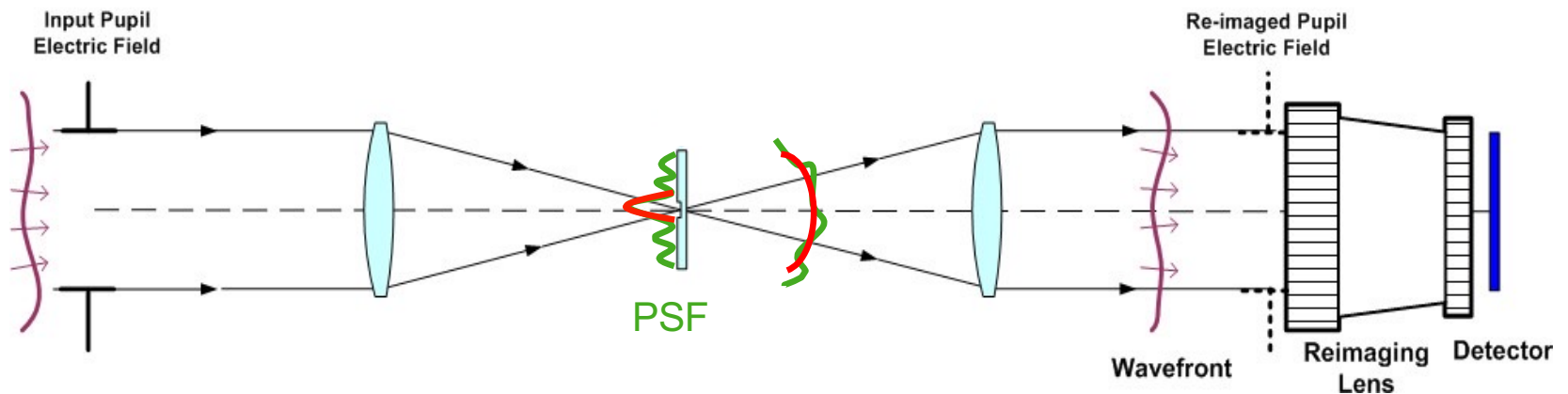


Without modulation:
linear over spot width



With modulation: linear
over modulation width

Zernike phase contrast technique: converting phase variations into intensity measurements imaged on a detector



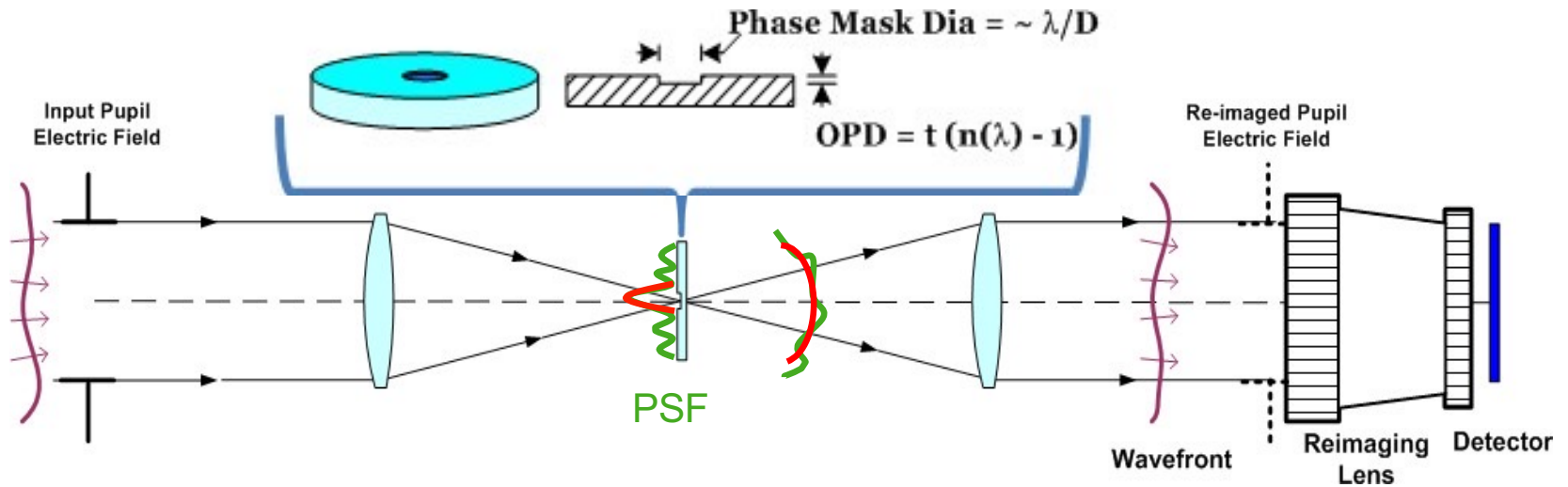
Brightfield

Original Phase Contrast
Photomicrographs of
Human Cells by Frits
Zernike in 1930s



Phase Contrast

Zernike phase contrast technique: converting phase variations into intensity measurements imaged on a detector



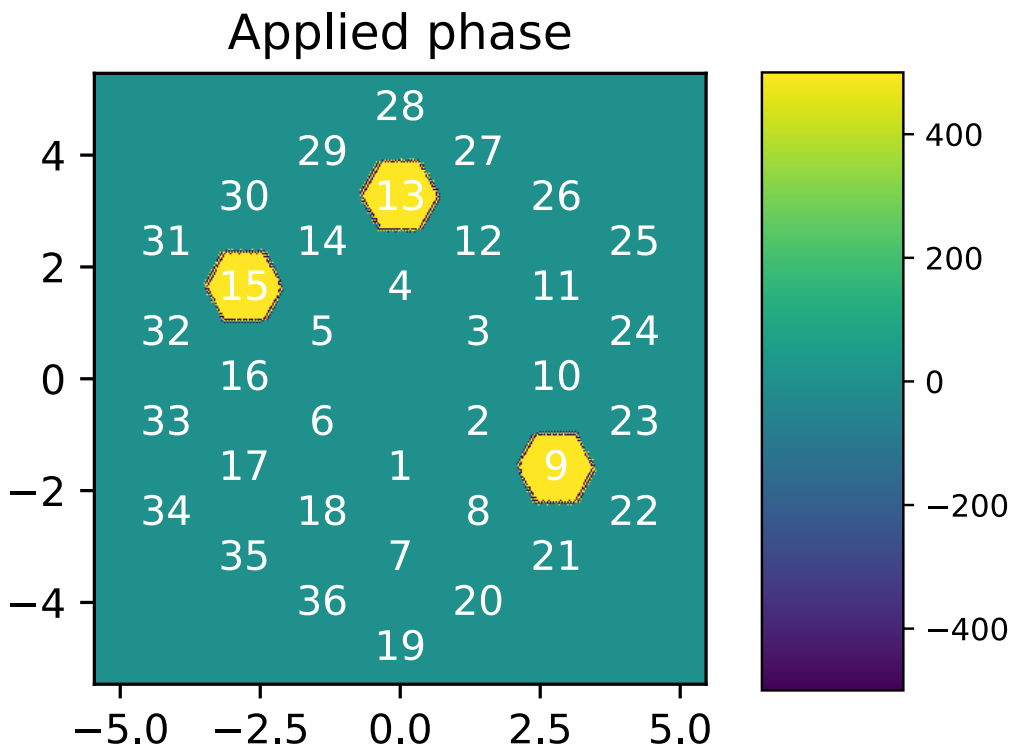
sensitivity

dynamics

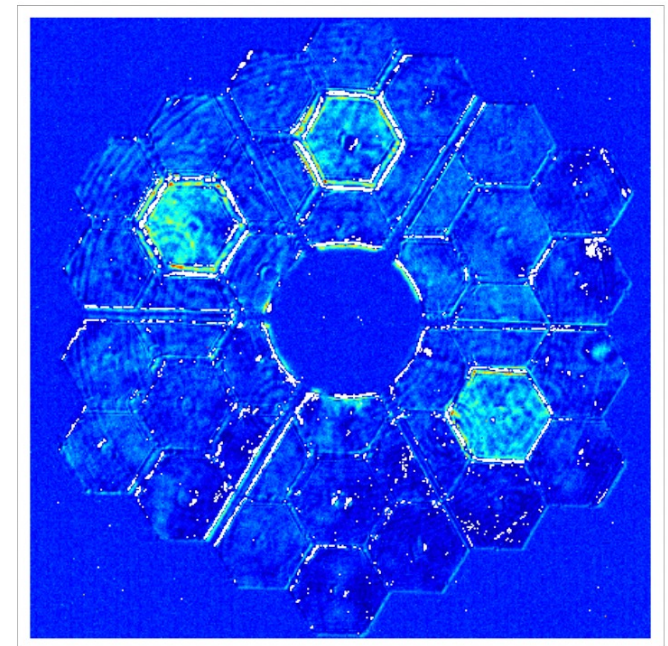
VERY sensitive but
SMALL dynamic range



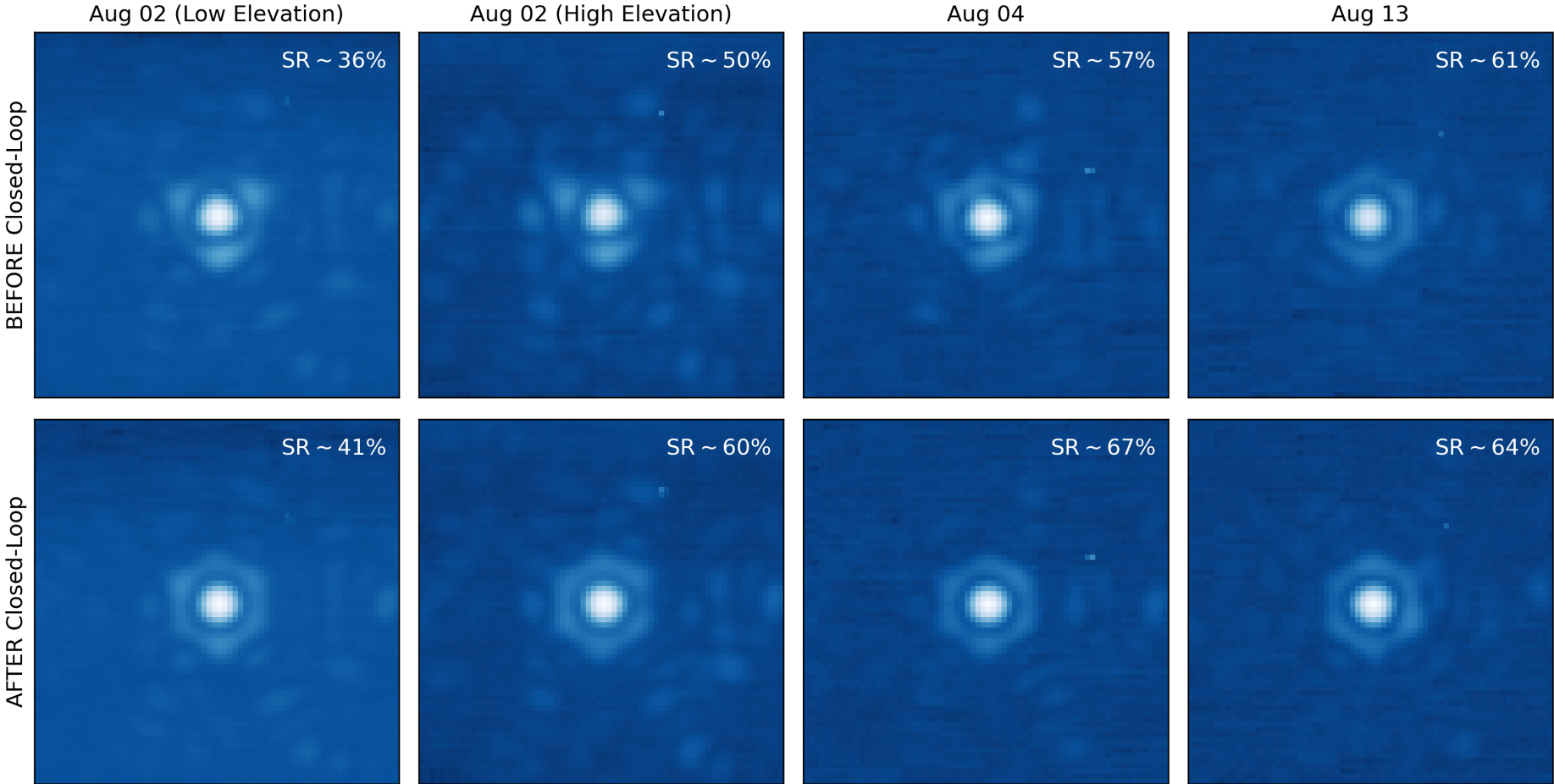
Using a ZWFS to characterize the cophasing of Keck's Segmented Primary Mirror: van Kooten et al. 2022



Zernike Image



Using a ZWFS to improve the cophasing of Keck's Segmented Primary Mirror: Salama et al. 2024

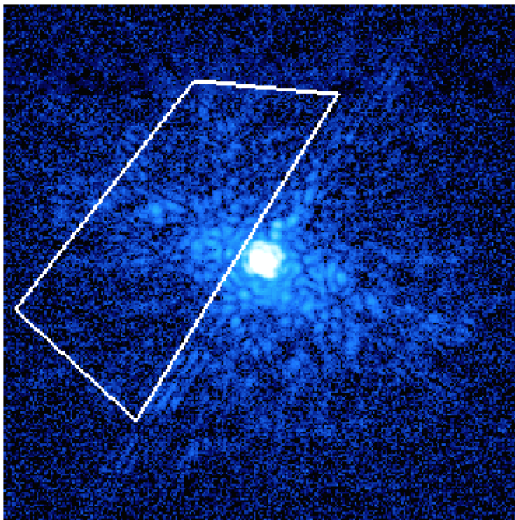


Focal Plane wavefront sensing

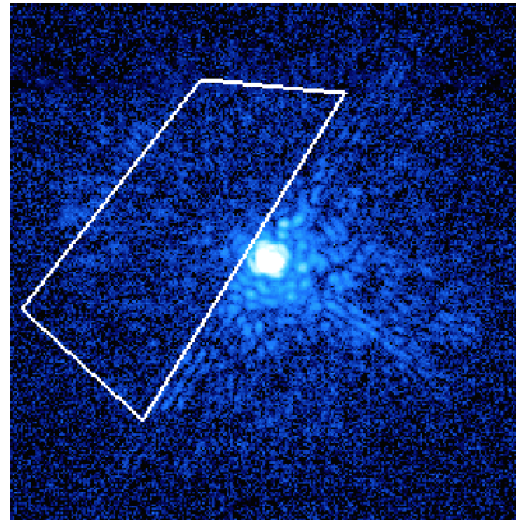
- Focal plane WFS: wavefront properties are deduced from intensity measurements made at or near the focal plane
- Why is focal plane wavefront sensing hard?
 - Recall that the intensity is $E \cdot E^*$, so when you look at e.g. an image of the PSF you've lost the sign information from the phase
 - So, e.g. if your PSF is defocused you can't know which side of focus it's on
 - You need some kind of variation or "diversity" if you want to reconstruct the phase from an intensity image
- Jovanovic et al. 2018 is a nice overview of FPWFS techniques

Speckle Nulling

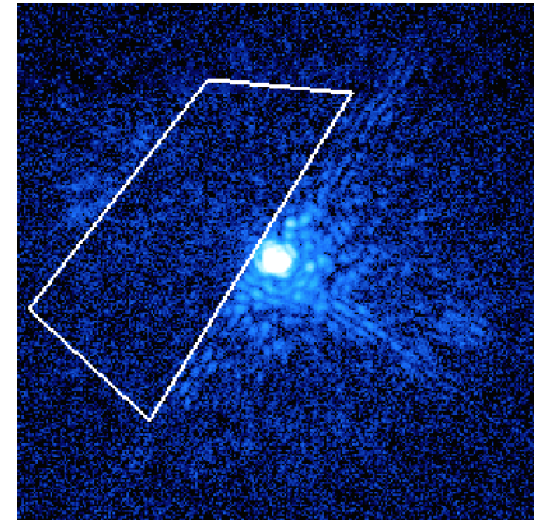
- Coronagraphs null the diffraction-limited component of the PSF
- Non-common path aberrations create slowly-evolving speckles
- By putting sine waves of the corresponding frequency on the DM, you can null these speckles



(a) Initial speckle field



(b) Fourth iteration

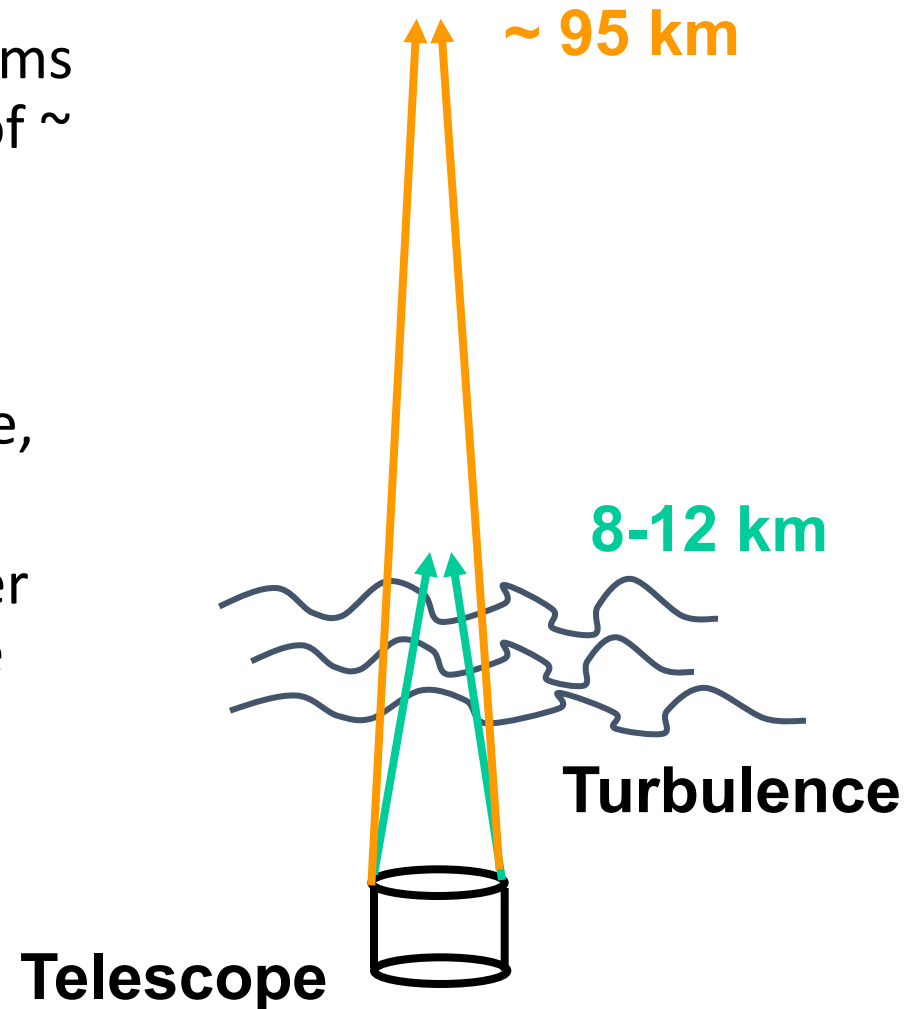


(c) Ninth iteration



Two types of laser guide stars in use today: “Rayleigh” and “Sodium”

- **Sodium guide stars:** excite atoms in “sodium layer” at altitude of ~ 95 km
- **Rayleigh guide stars:** Rayleigh scattering from air molecules sends light back into telescope, $h \sim 10$ km
- Higher altitude of sodium layer is closer to sampling the same turbulence that a star from “infinity” passes through



Summary

- Wavefront sensing and control is necessary for both ground and space-based telescopes
- A wavefront sensor is an optical device which transforms phase into intensity
- Wavefront sensors come in many genres, including pupil plane and focal plane sensors.
- Wavefront sensors and coronagraphs are two sides of the same coin
- To learn more, join us in Santa Cruz for the AO Summer School in August! Register here by the end of this week:
cfao.science.ucsc.edu/ao-summer-school